

Project 49

Urban Air Mobility Noise Reduction Modeling

Penn State

PI: Kenneth S. Brentner

PM: Rick Riley

Cost Share Partner: Continuum Dynamics, Inc/Penn State



Objective:

- Develop a first-principles noise modeling system for future UAM aircraft with varied configurations
- Produce noise database for notional UAM configurations for hover, transition, cruise
- Identify configuration changes and operational strategies that minimize acoustic impacts

Project Benefits:

- Initial capability to analyze UAM acoustics
- Understanding of UAM noise characteristics
- Identification of noise reduction opportunities
- Low noise design tool for the UAM industry
- Initial UAM noise data for input to Advanced Acoustic Model, which can provide input to AEDT

Research Approach:

- Build on success of helicopter noise prediction system developed under ASCENT Projects 6 & 38:
 - Couple flight simulation, aerodynamic modeling (CDI's CHARM), and PSU-WOPWOP
- Tailor approach to unique characteristics of UAM by modeling flight dynamics of distributed electric propulsion vehicles including multiple propellers and rotors with PSU-DEPSim
- Develop low noise UAM trim strategies

Major Accomplishments (since last meeting):

- Analysis of departure maneuver for lift-plus-cruise eVTOL
 - Aircraft transitioning from hover to cruise while gaining altitude
- Time-varying broadband noise implementation in system made more robust
 - Validating prior to external release
- Conducted literature review of turbulence ingestion noise models to implement in system

Future Work / Schedule:

- Implement models of broadband ingestion noise generated by aerodynamic interactions

Presentation Outline

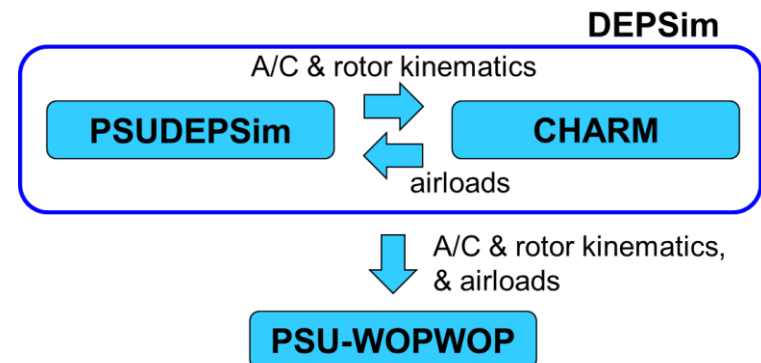


- Motivation
- Noise during transition maneuver
 - Dealing with over-actuated controls
 - Demonstration of impact of trajectory on acoustic impact
- Time-varying broadband noise
- Summary:
 - Accomplishments
 - Future work

Motivation

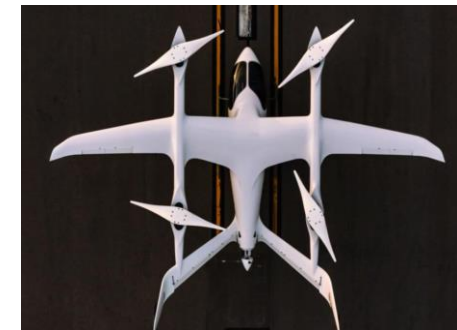
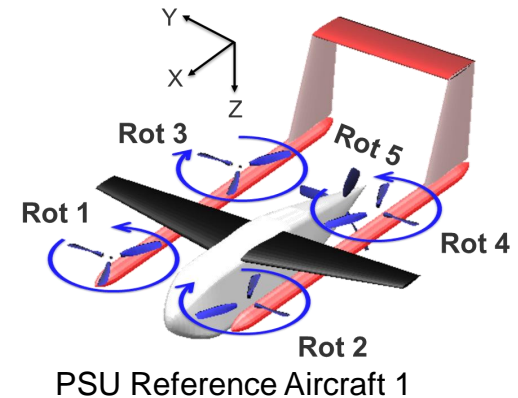
- Noise is widely recognized as one of the foremost barriers to development and public acceptance of UAM operations
- Information about acoustic characteristics of UAM is needed:
 - To design quiet configurations
 - To understand how to operate UAM quietly
 - To inform the approach to noise certification
 - To understand the impact on communities
- Development of robust noise prediction system:
 - PSUDEPSim: flight simulation code for DEP aircraft
 - CHARM: aeromechanics modeling code by CDI
 - PSU-WOPWOP: acoustic propagation solver
- DEPSim/PSU-WOPWOP system enables systematic investigation of UAM configurations, flight physics, and noise emission

- System allows investigating:
 - Fundamental noise mechanisms of novel variable rotational speed rotors
 - Nature of multi-rotor noise
 - Trim strategies of compound aircraft

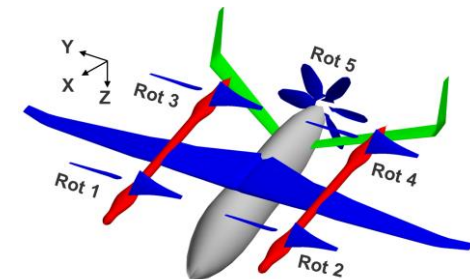


Aircraft models analyzed

- PSU Reference Aircraft 1
 - Weight = 1000 lbf
 - Notional geometry
- PSU Reference Aircraft 2
 - Weight = 7000 lbf
 - Based on public information available on Beta Alia aircraft
- Both aircraft have
 - 4 lift rotors
 - 1 cruise pusher propeller
 - 1 wing for active lift (and propulsion)



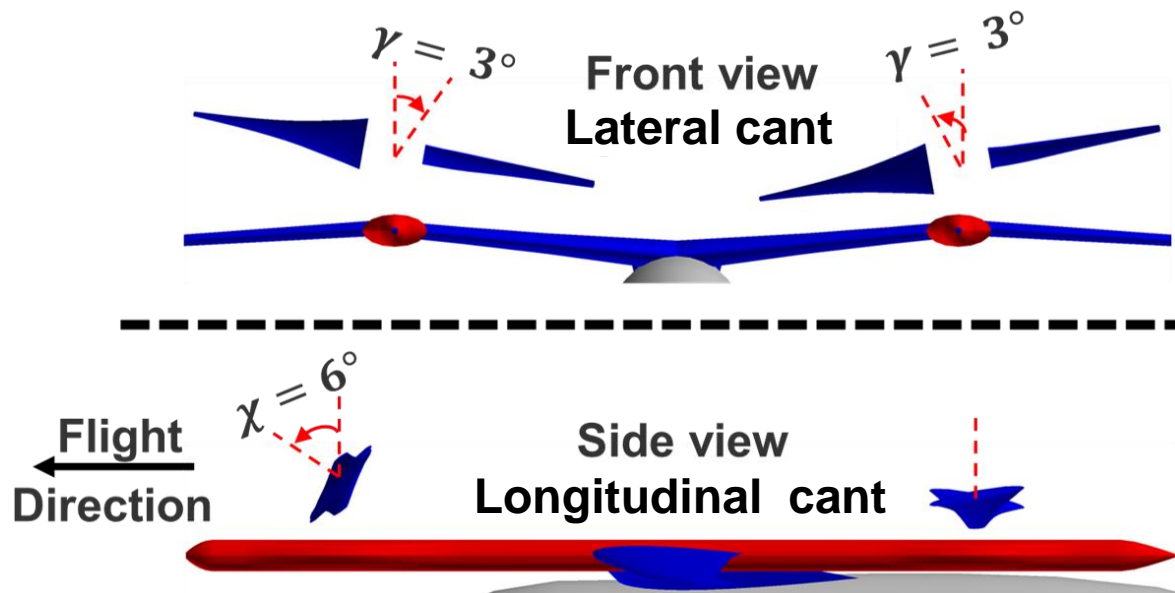
Beta Alia (source: evtol.com)



PSU Reference Aircraft 2

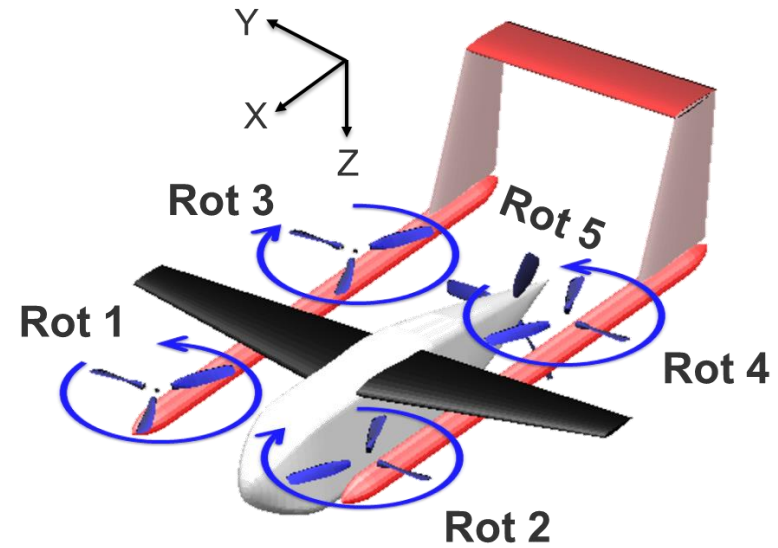
PSU Reference Aircraft 2: unique design

- Lift rotors are canted:
 - Rotor lateral cant 3°
 - Front rotors longitudinal cant 6°
- Rotor cant is known to improve controllability in transition
 - Lateral cant improves yaw control authority and stability
 - Longitudinal cant provides a component of lift rotor thrust in the flight direction during transition
- Impact of rotor cant on noise has not been studied yet



Low-noise lessons learned

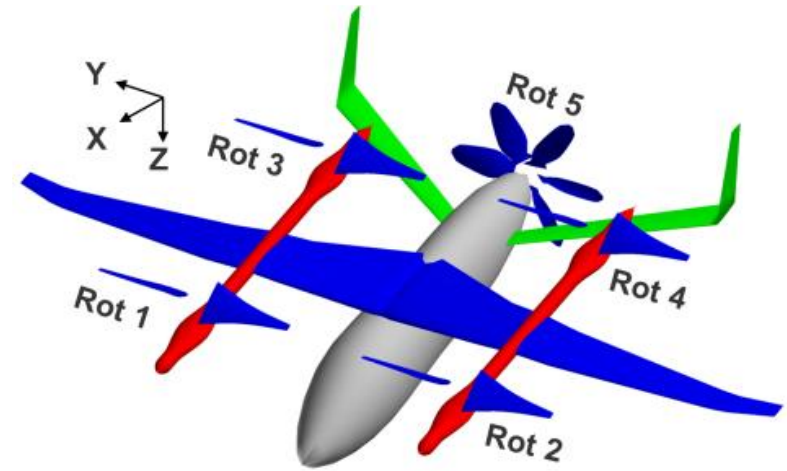
- Thrust on lift rotors (Rot 1 – 4) should be kept as low as possible
 - Helps reduce the required thrust to balance aircraft weight during transition
 - Results in lower operational tip-Mach number (important for noise)
- Rotor blades operating in **stall** at low tip-Mach number have significant contribution to self-noise
 - Turbulent boundary layer scattering via the trailing edge
 - Bad for performance/aerodynamics too



PSU Reference Aircraft 1

Low-noise strategy: Lift + Cruise Design

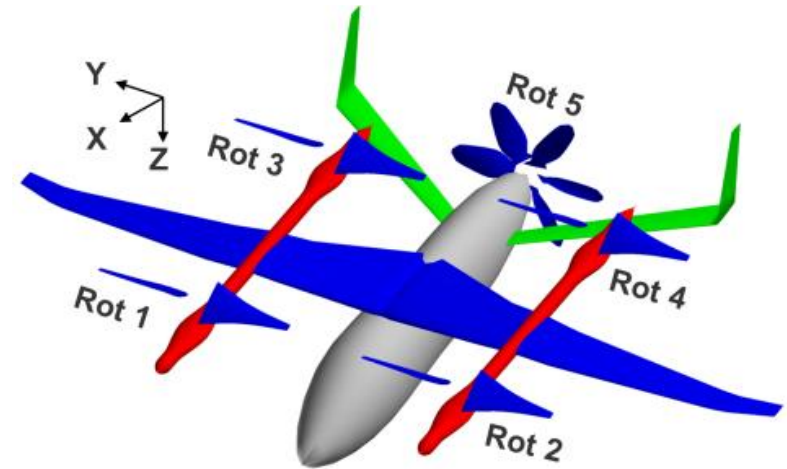
- Highest wing lift as soon as possible
- Wing lift proportional to:
 - Flight speed ($\sim V_\infty^2$)
 - Angle of attack (directly dependent on aircraft pitch)
- No rotor stall
 - Lift rotor thrust control strategies need to be adapted for no stall
 - Variable pitch, constant RPM
 - Variable RPM, constant pitch
- Rotors larger than 6ft diameter not well controlled using variable RPM scheme
 - Current aircraft rotor diameter is 12 ft



PSU Reference Aircraft 2

Low-noise strategy: Lift + Cruise

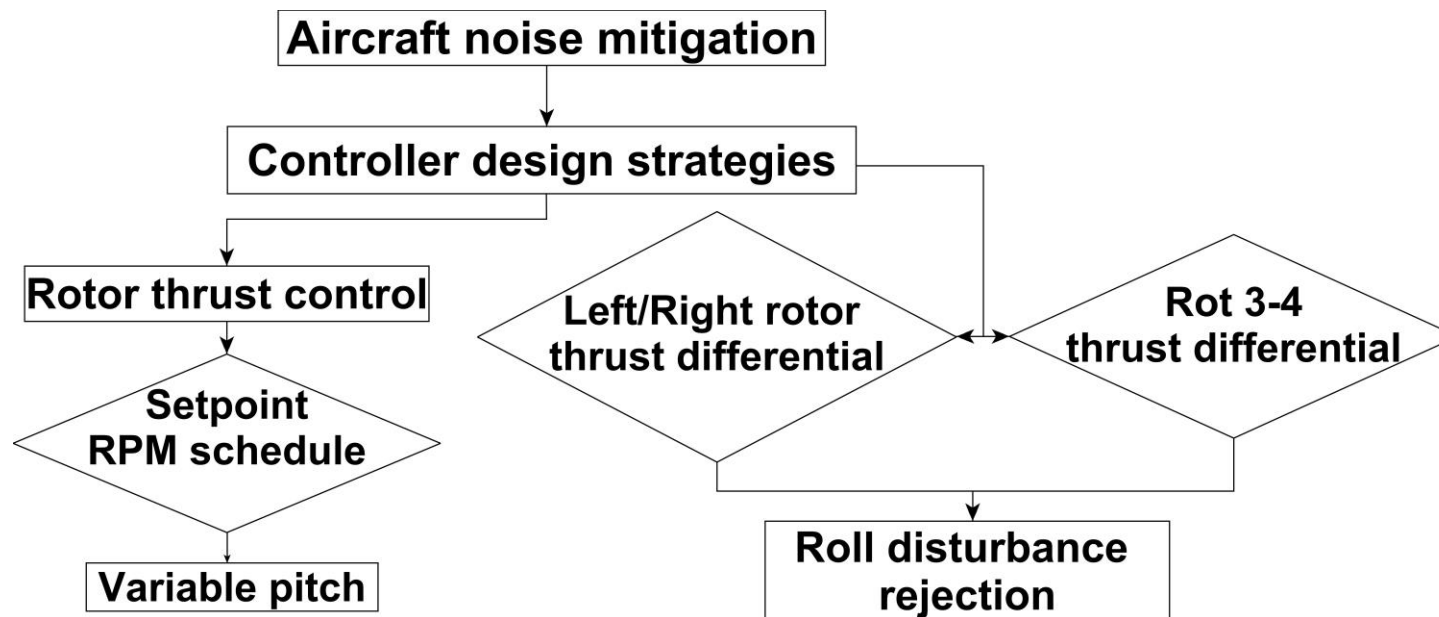
- **Transition maneuver:**
 - Maneuver that goes from vertical flight to cruise
 - Control of vehicle
 - Variable pitch
 - Constant RPM
 - “Constant RPM” – RPM set at different **setpoints** throughout maneuver
 - Dependent on flight condition
 - Advantage of electric motors
 - Rotor designs are usually optimal for a small range of flight conditions



PSU Reference Aircraft 2

Noise mitigation strategies

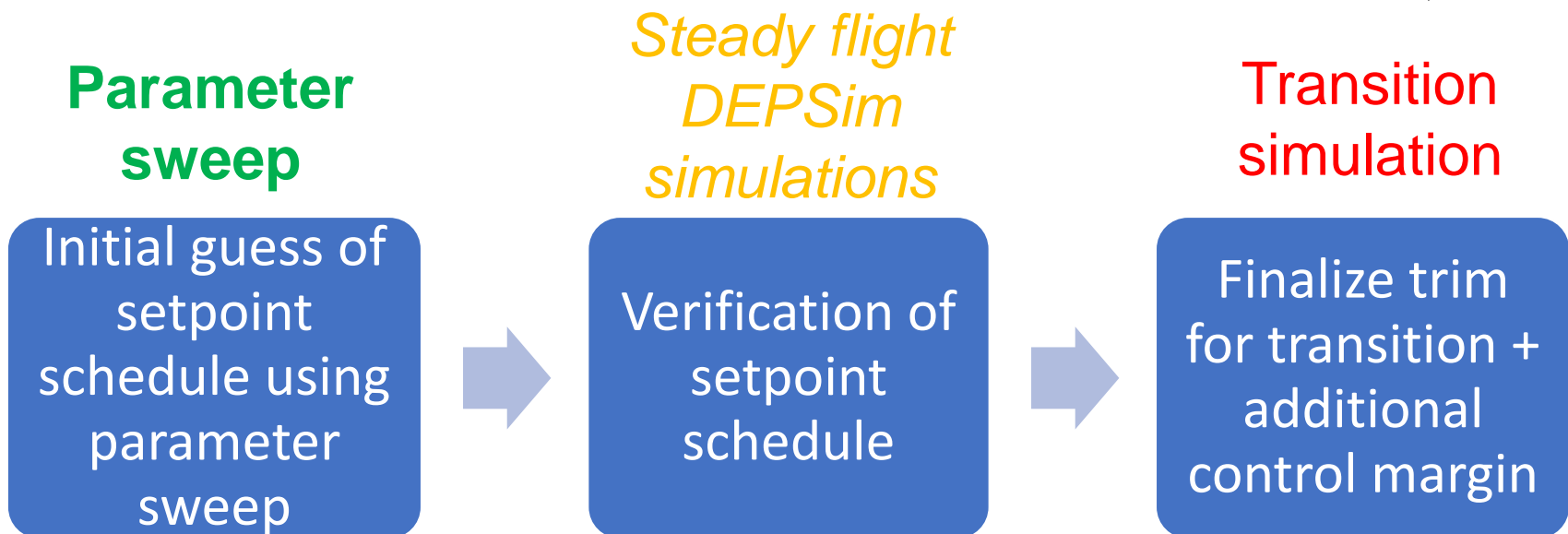
Multi-rotor aircraft design and availability of multiple lift rotor thrust control schemes allows a diverse approach in noise mitigation



Parametric sweep strategy

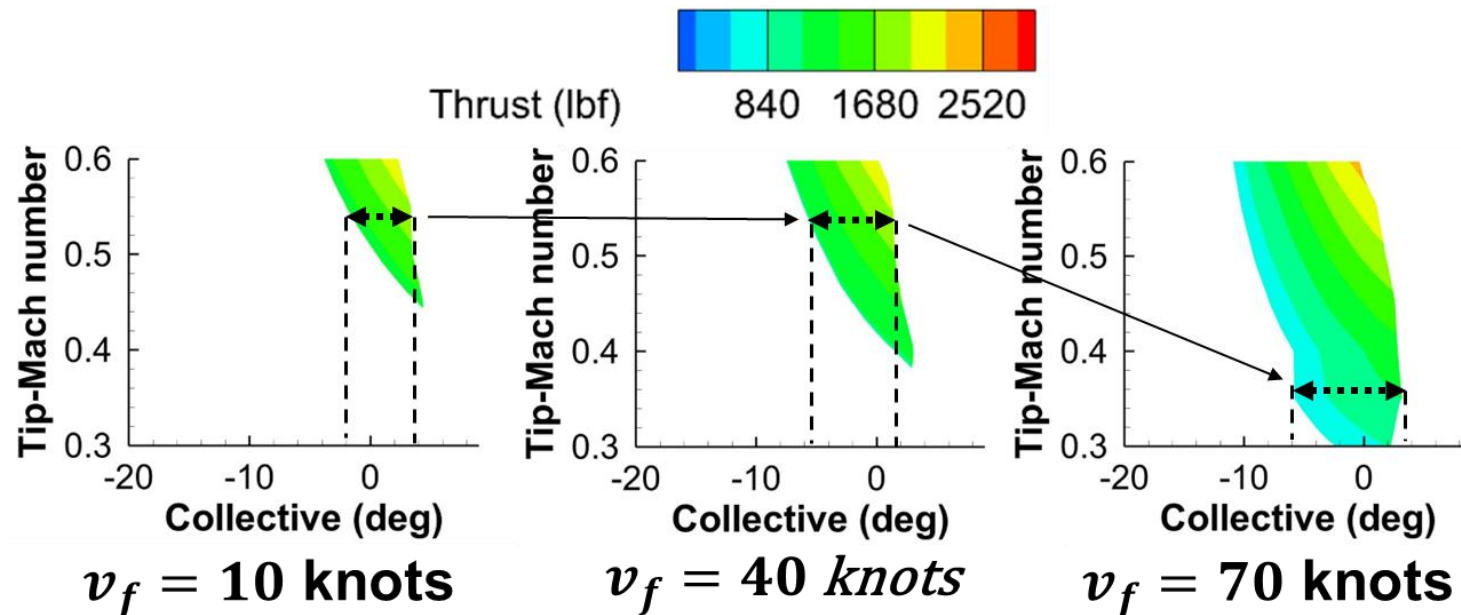
- Goal: Minimize computational cost associated with finding setpoint schedule suitable for controllability, acoustics and performance

Increasing computational cost



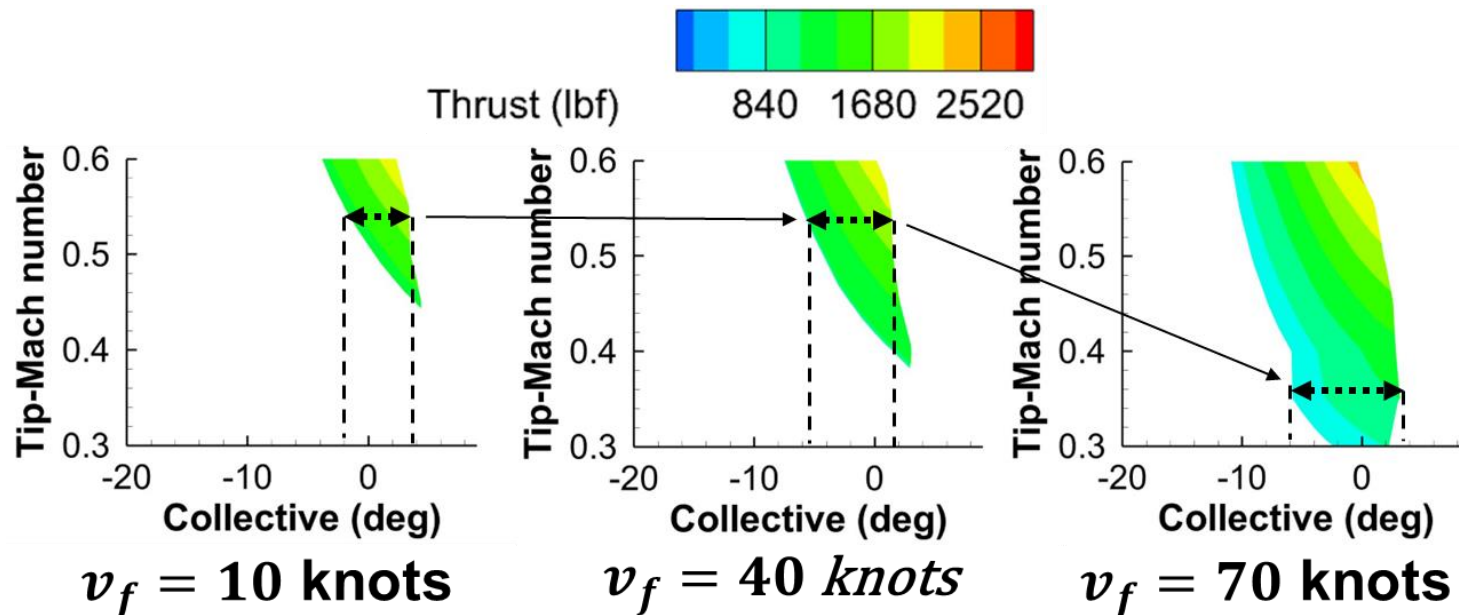
Setpoint schedule: Initial guess

- Isolated lift rotor parametric sweep exploration space:
 - Tip-Mach: 0.3 to 0.6
 - Rotor collective pitch: -20° to 9°
 - Velocity: 10, 20, 30, 40, 50, 60, 70 knots at $\theta = 8^\circ$
- Metrics evaluated: rotor thrust, power, stall
 - Conditions with rotor stall rejected on account of noise



Setpoint schedule: Initial guess

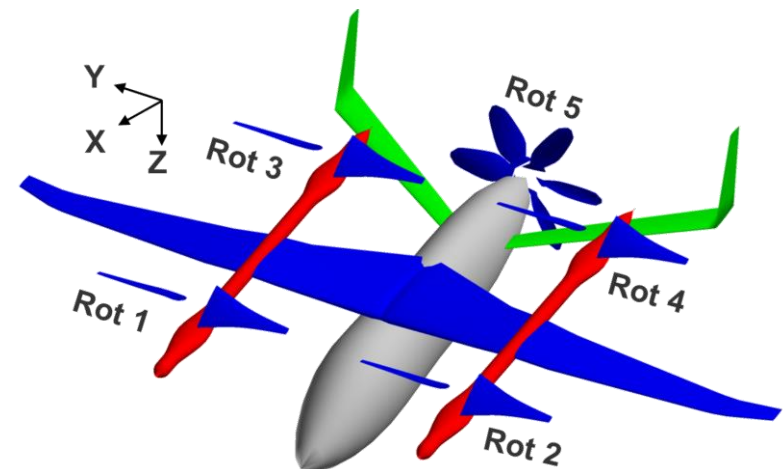
- Metrics evaluated: rotor thrust, power, stall
 - Conditions with rotor stall rejected on account of noise
 - Rotor thrust must be enough to balance aircraft weight
- Rotor thrust estimate = $\frac{\text{Aircraft weight} - \text{Wing lift}}{\text{number of lift rotors}}$
 - Works well in predicting the range of rot 1 – 4 collective pitch angles for steady flight conditions



Setpoint schedule: Initial guess

- Comparison of initial guess with DEPSim steady simulations

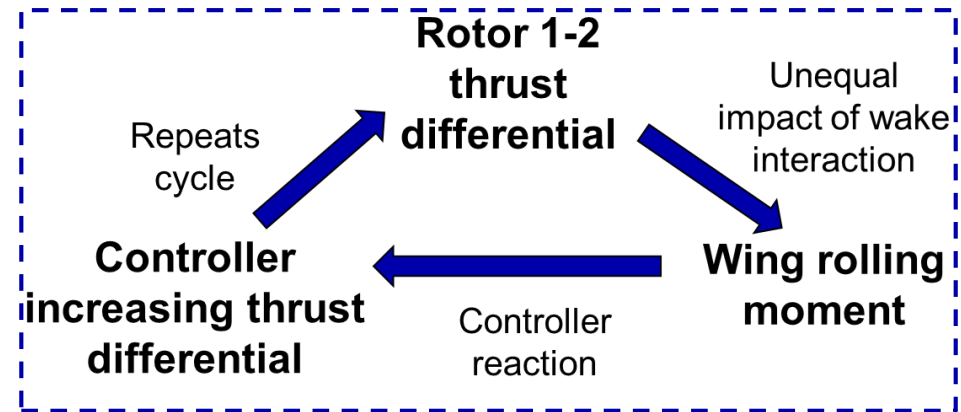
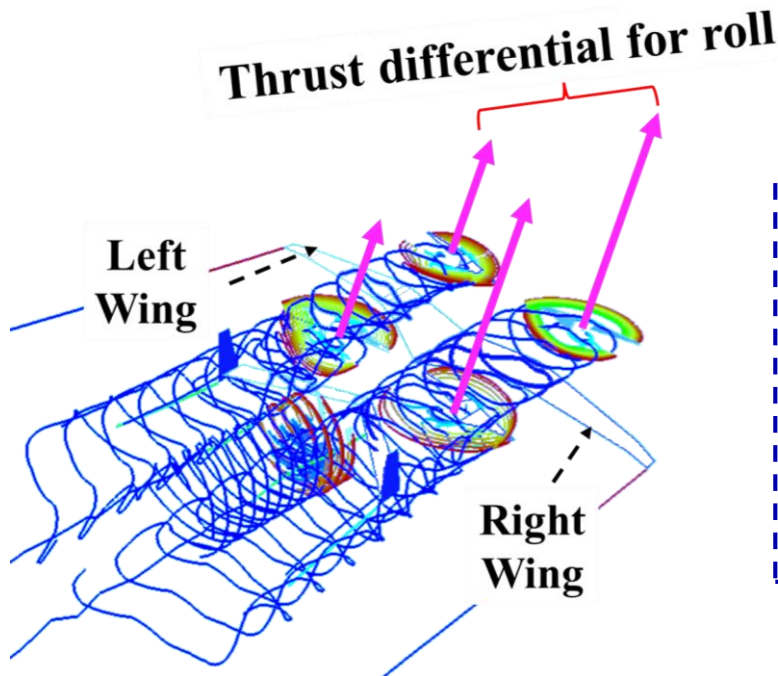
v_f (knots), tip-Mach	10, 0.55	40, 0.55	70, 0.35
Collective range from sweep (deg)	-2 to 4	-6 to 2	-6 to 4
DEPSim collective Rot 1,2,3,4 (deg)	1.8, 1.5, 2.6, 2.3	-4.8, -3.9, 1, 0.2	0.6, -11 , 2.5, -2.8



This discrepancy has a reason.

Role of interaction in dynamics

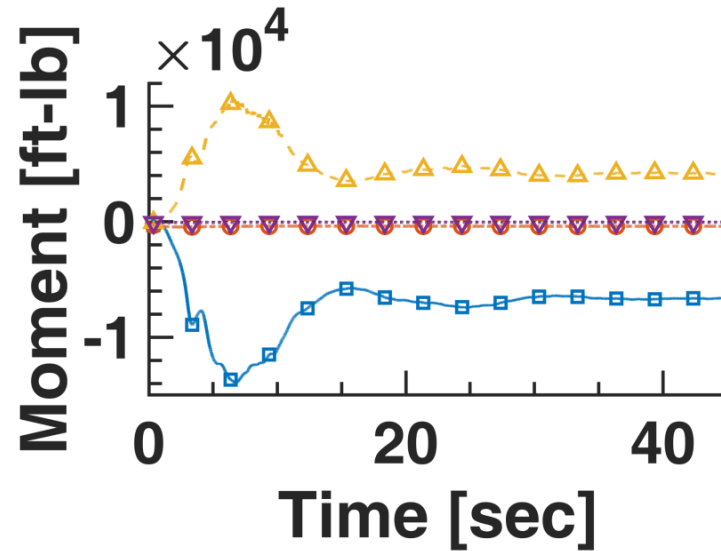
- DEPSim controls aircraft roll disturbance using the difference in thrust between rotors on each side
 - Rot 1 – Rot 2 thrust & Rot 3 – Rot 4 thrust



Rolling Moment: 70 knots

- Break moment cycle by changing how the controller compensates for rolling moment
 - Do not use rotors 1-2 thrust differential for roll rejection!
- Steady flight simulation 70 knots
 - Controller starts without knowledge of interactions
 - Interaction feedback starts around 5 seconds
- “CHARM Off” aero model has no aerodynamic interactions
 - Magnitude of rolling moment is much lower

■ Total Rotor Moment - CHARM On ⊖ Total Rotor Moment - CHARM Off
▲ Total Wing Moment - CHARM On ▼ Total Wing Moment - CHARM Off

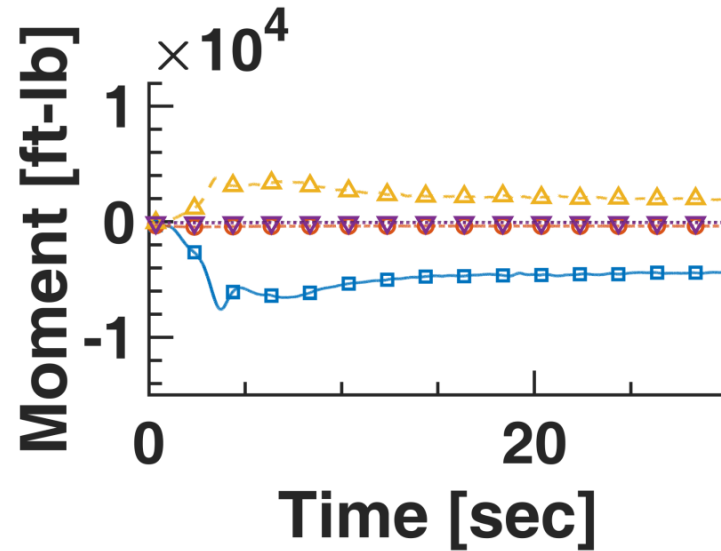


Roll moment vs Time

Rolling Moment: 70 knots

- Same steady flight simulation
- **Change in controller design**
 - Rotor 1,2 no longer involved in roll rejection
- Notice large reduction in wing and rotors moments
 - Improvement in controllability and performance
 - No significant change in noise

■ Total Rotor Moment - CHARM On ⊖ Total Rotor Moment - CHARM Off
▲ Total Wing Moment - CHARM On ▼ Total Wing Moment - CHARM Off



Roll moment vs Time

Setpoint schedule: Initial guess

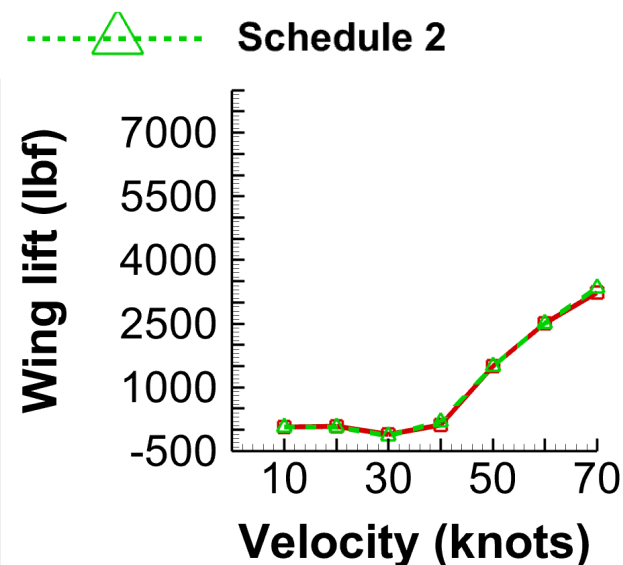
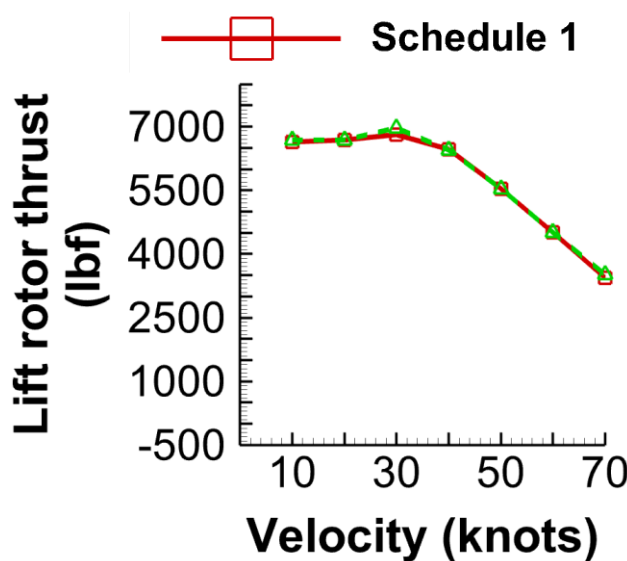
- Initial guess:
 - Schedule 1 expected to work
 - Schedule 2 used to verify whether schedule 1 is the lowest tip-Mach number that maintains reasonable controllability
 - 14 steady flight simulations

Velocity (knots)	Schedule 1	Schedule 2
10	0.55	0.50
20	0.55	0.50
30	0.55	0.50
40	0.55	0.50
50	0.50	0.50
60	0.45	0.45
70	0.35	0.35

Verifying setpoint schedule: Steady flight DEPSim

- Wing lift starts to increase significantly after 40 knots
- Note the dip in wing lift around 30 knots
 - Due to wakes from the front two rotors
 - Wakes creates downwash on wing
 - Downwash results in negative lift!

Velocity (knots)	10	20	30	40	50	60	70
Schedule 1	0.55	0.55	0.55	0.55	0.50	0.45	0.35
Schedule 2	0.50	0.50	0.50	0.50	0.50	0.45	0.35



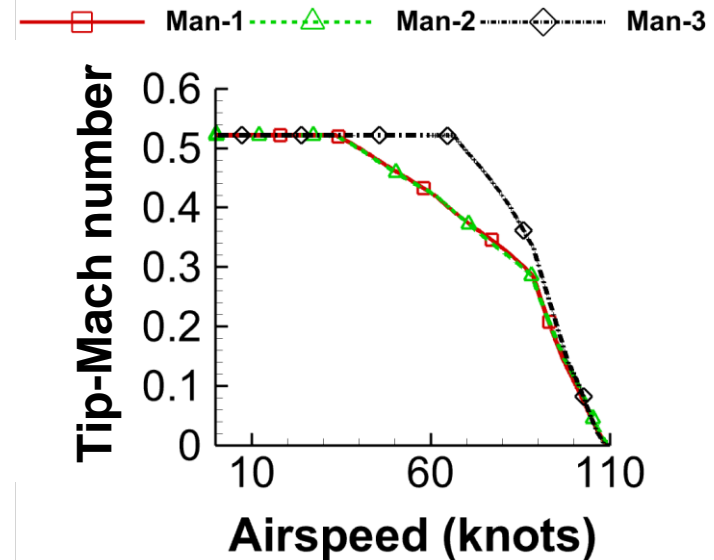
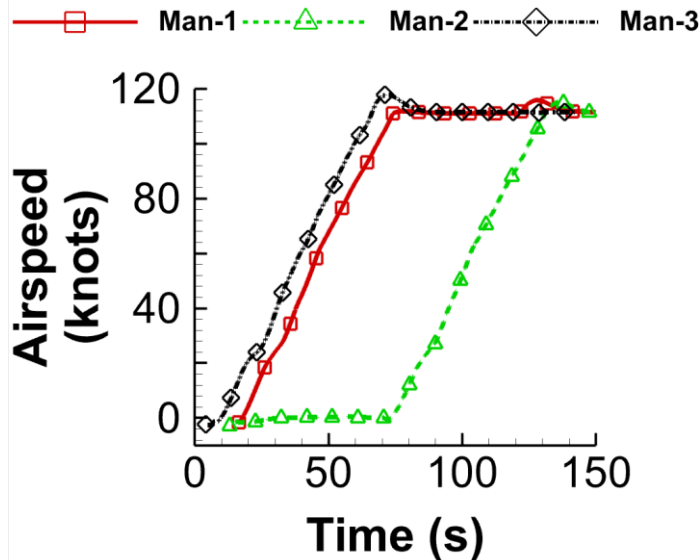
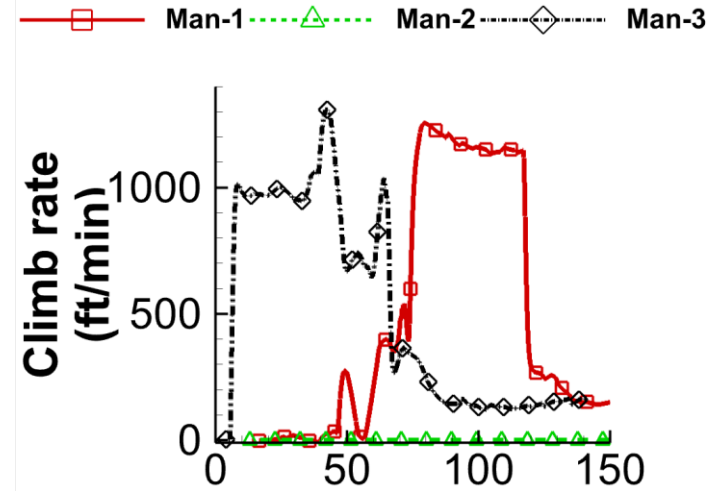
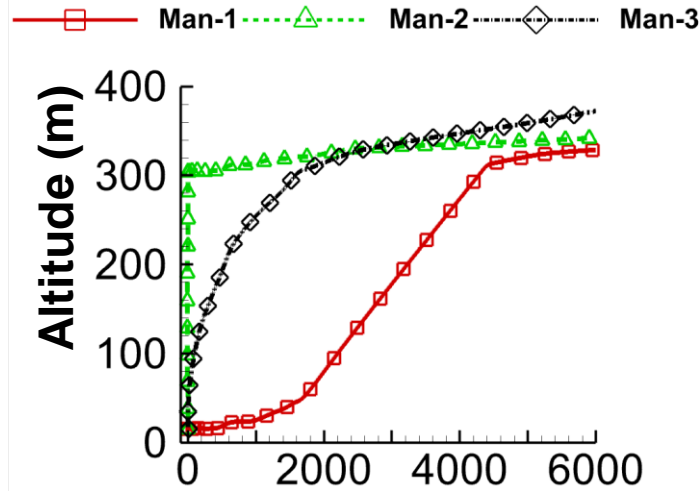
Departure maneuver



- Departure maneuver was simulated using Penn State eVTOL Noise prediction system
 - This maneuver makes the aircraft transition from rotorcraft mode (**hover**) to fixed-wing airplane mode (**cruise**)
- Three departure maneuvers: all start at hover, 50 ft altitude, and end at 110 knots, 1000 ft altitude, 20,000 ft downrange
 - **Level acceleration:** Hover -> 0.1g low altitude level acceleration to 110 knots (rotors off by 110 knots), then climb to 1000 ft at 1000ft/min
 - **Axial climb:** Hover -> 1000ft/min climb to 1000 ft -> 0.1g level acceleration to 110 knots
 - **Continuous climb:** Hover-> 0.1g level acceleration + 1000ft/min climb -> Rotors off at 110 knots -> Climb to 1000 ft in aircraft mode
 - Higher bias schedule due to higher demands of thrust for continuous climb rate + level acceleration

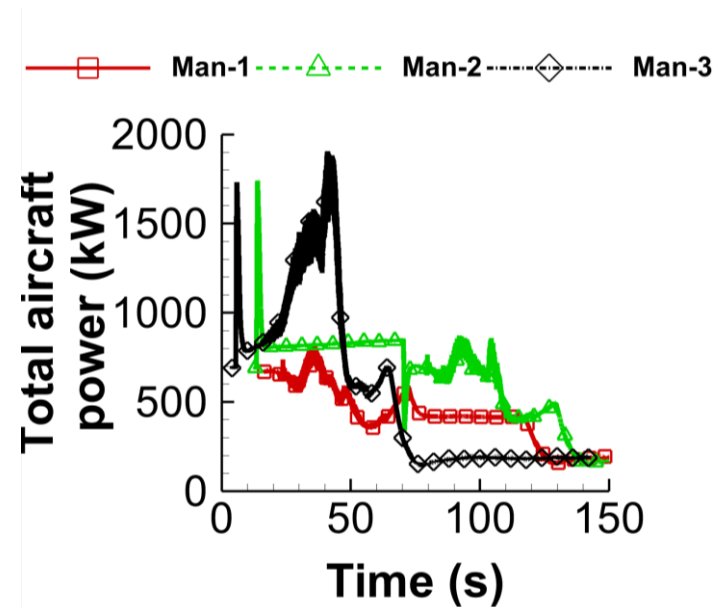
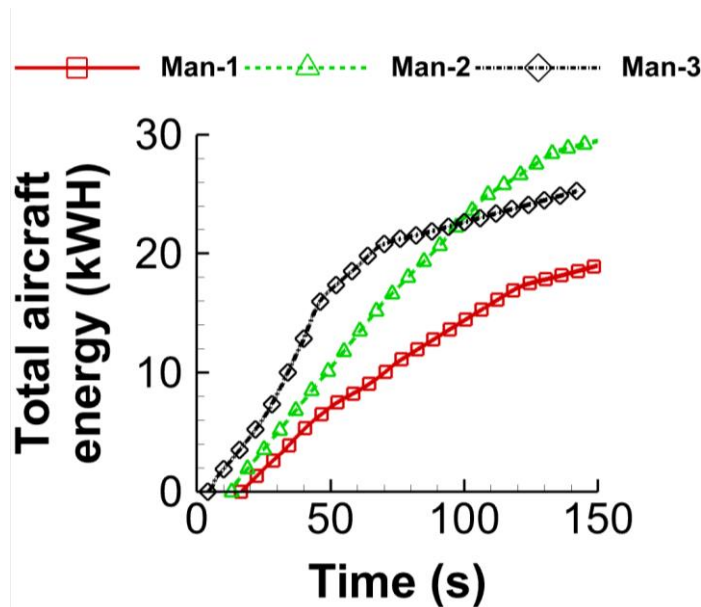
Departure maneuver: Trajectory

- **Level acceleration: Man-1; Axial climb: Man-2; Continuous climb: Man-3**



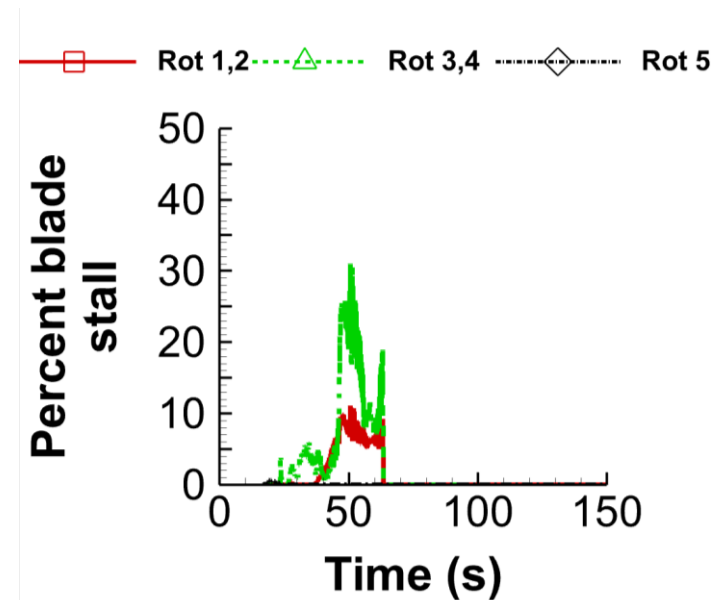
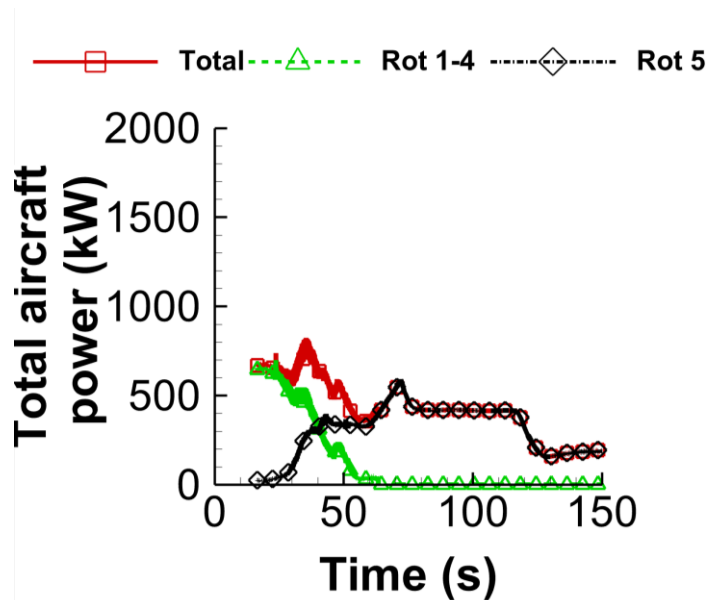
Departure maneuver: Energy, Power

- **Level acceleration:** Man-1: Lowest energy, lowest peak power
- **Axial climb:** Man-2: Highest energy, second highest peak power
- **Continuous climb:** Man-3: Second highest energy, highest peak power



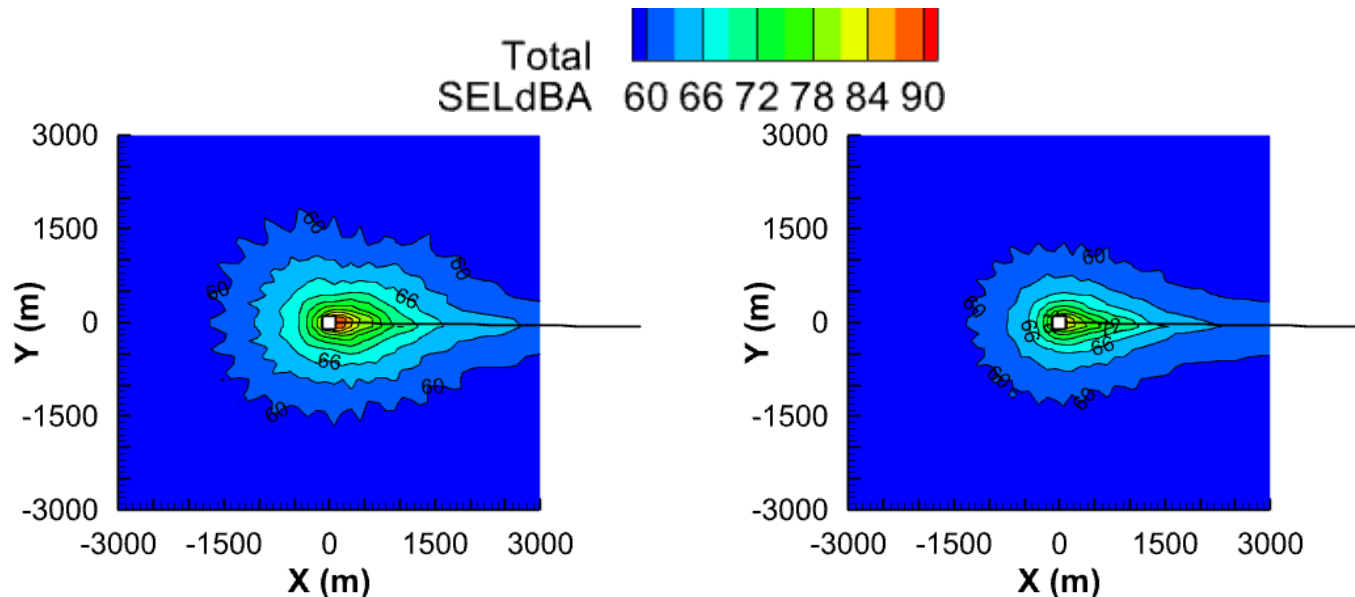
Departure maneuver: Power, Stall

- **Level acceleration:** Lowest energy, lowest peak power
 - Lift rotor power higher than pusher prop in level acceleration (it balances weight)
 - Pusher prop increases during climb in aircraft mode
- Lift rotor blade stall: 10 – 30 %



Departure maneuver: Noise

- **Level acceleration:** Lowest energy, lowest peak power
 - Lift rotor stall: 10 – 30 %
- Stall is not playing a major role in noise
 - Setpoint schedule works
- Noise levels high along trajectory (marked in black)

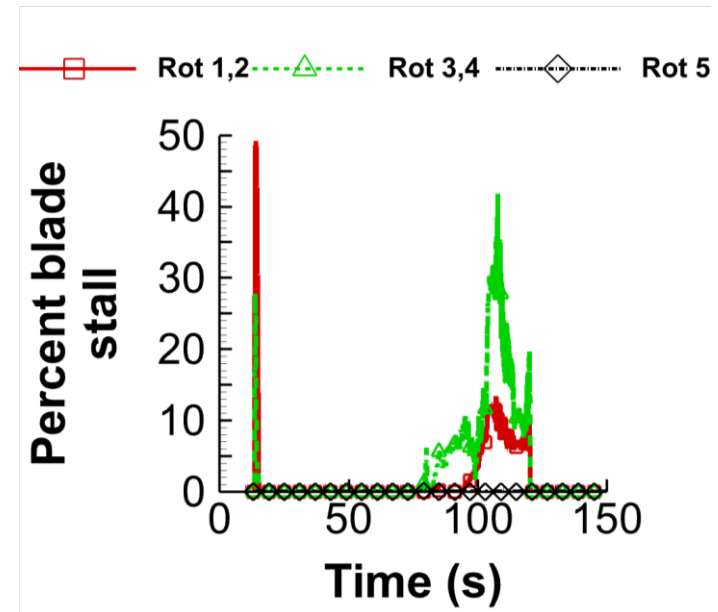
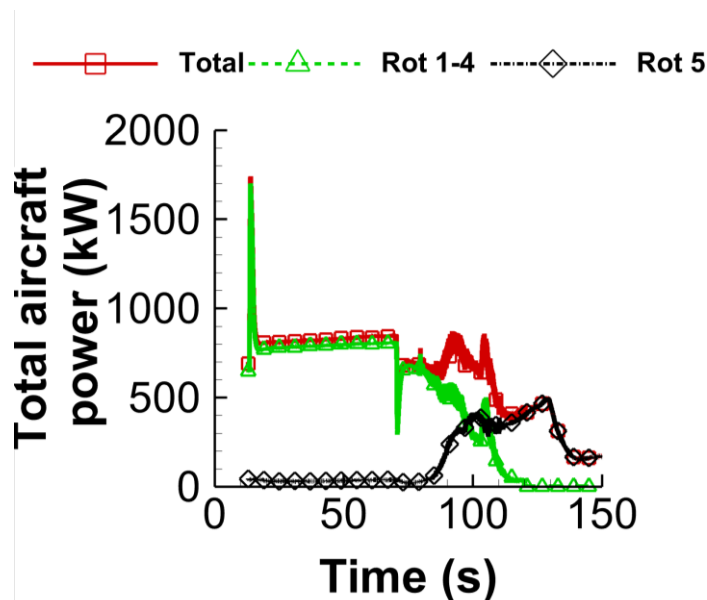


Total noise

Total noise excluding stall from BPM

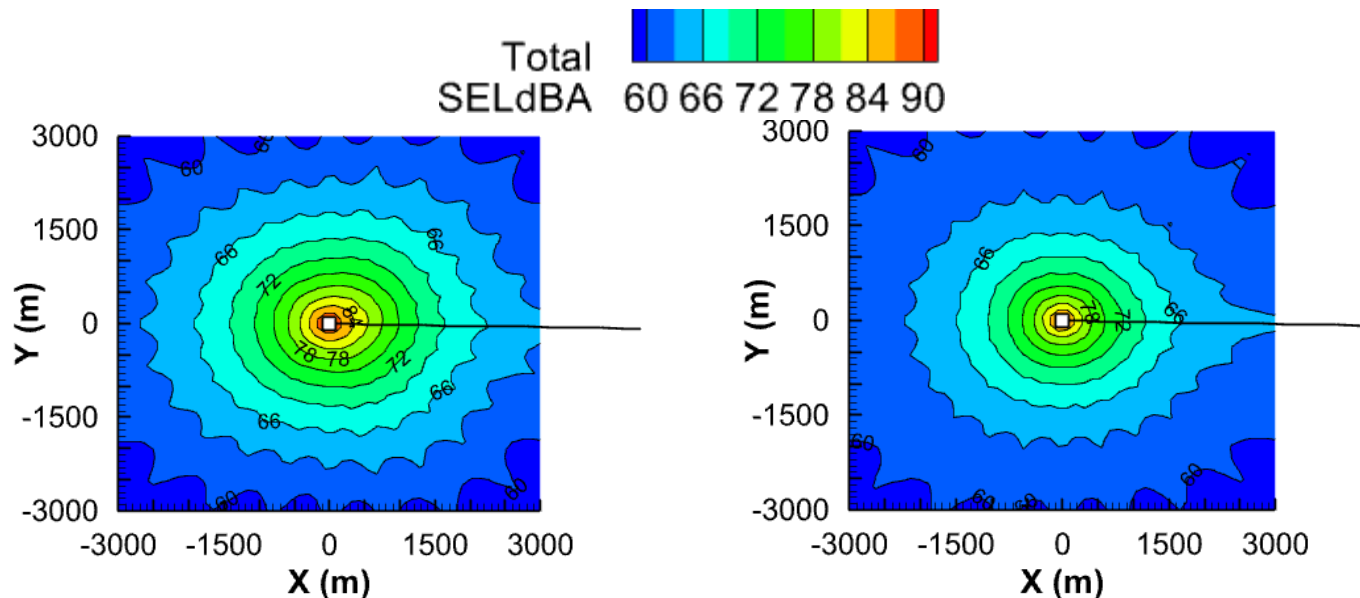
Departure maneuver: Power, Stall

- **Axial climb:** Highest energy, second highest peak power
 - High lift rotor power for majority of flight: Because its responsible for climb
 - Spike in power is when the controller ramps rotor collective to have a short period of vertical acceleration to gain 1000 ft/min climb rate
- Lift rotor stall: 10 – 40 %



Departure maneuver: Noise

- **Axial climb:** Highest energy, second highest peak power
 - Lift rotor stall: 10 – 40 %
- Stall is not playing a major role in noise
 - Setpoint schedule works
- Noise levels high throughout plane: aircraft is in rotorcraft mode for longest time

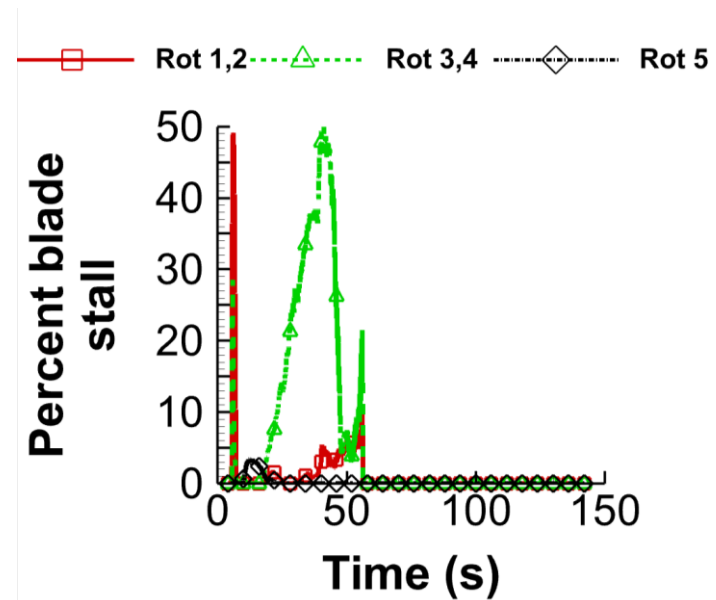
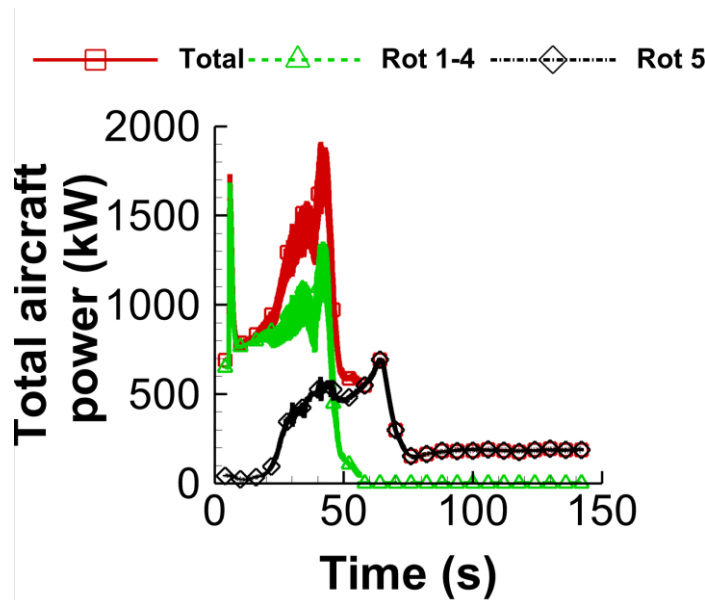


Total noise

Total noise excluding stall from BPM

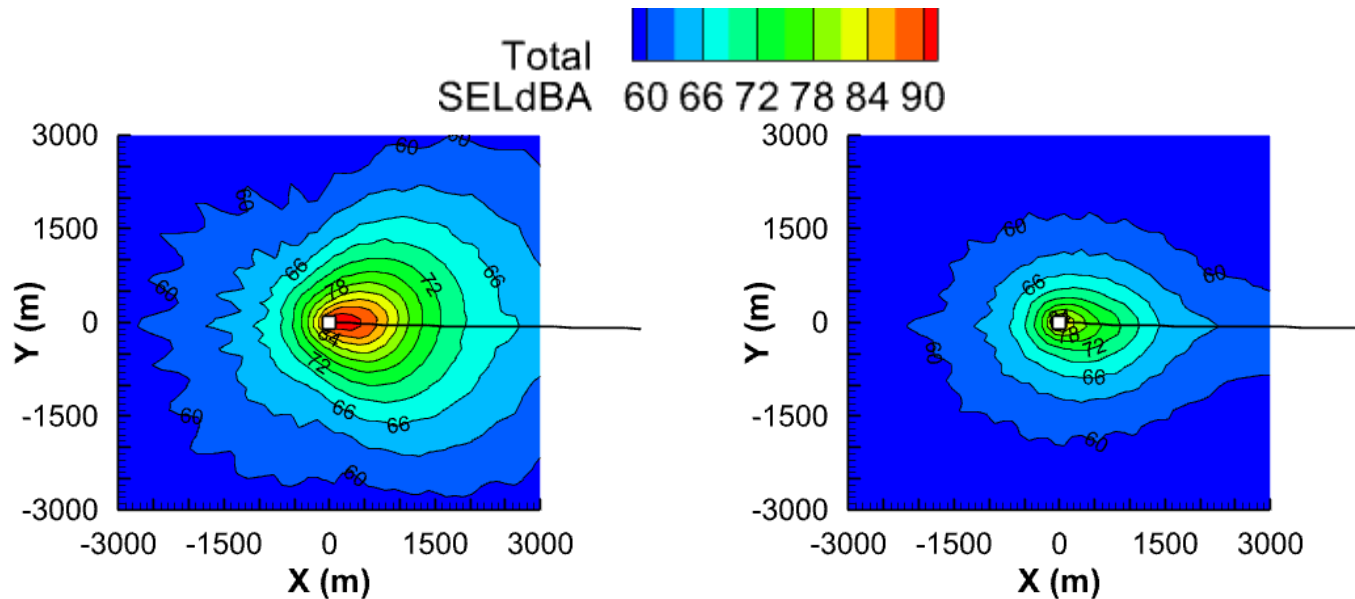
Departure maneuver: Power, Stall

- **Continuous climb:** Second highest energy, highest peak power
 - Climb + level acceleration leads to really high lift rotor power
 - Note higher sustained cruise prop power as it is contributing to climb
- Lift rotor stall: 10 – 50 %
 - Stalled for longer period of time



Departure maneuver: Noise

- **Continuous climb** : Second highest energy, highest peak power
 - Lift rotor stall: 10 – 50 %
- Stall is playing a major role in noise
 - Recall: Setpoint schedule was not developed for climb
- Noise levels similar to level acceleration when stall is excluded:
Low noise strategy is phasing off rotors as quickly as possible



Total noise

Total noise excluding stall from BPM

Time Variation of Broadband Noise

Background and Motivation



- Literature typically only analyzes broadband noise spectrum time-averaged over rotor revolution
- But spectrum varies within a rotor revolution, due to:
 - Edgewise flight
 - Aerodynamic interactions
- Time variation of broadband noise spectrum:
 - Not only affects noise levels, but likely perception [1]
 - Important for helicopters, but not well-understood
 - Must investigate for UAM – especially interactions

[1] A. Christian, J. Caston, and E. Greenwood, VFS 75th Annual Forum, 2019

Coding Status



- Past conference paper results [2, 3]:
 - Time-varying predictions **not** for external release (prototype code)
 - Did not post-process spectrum time history
- **Completed:** Fully implemented robust time-varying broadband noise prediction in PSU-WOPWOP
- **In progress:** Validation prior to external release

[2] Z. F. T. Gan, K. S. Brentner, and E. Greenwood, VFS 9th Biennial Autonomous VTOL Technical Meeting, 2021.

[3] Z. F. T. Gan, K. S. Brentner, and E. Greenwood, 28th AIAA/CEAS Aeroacoustics Conference, 2022.

Validation Approach

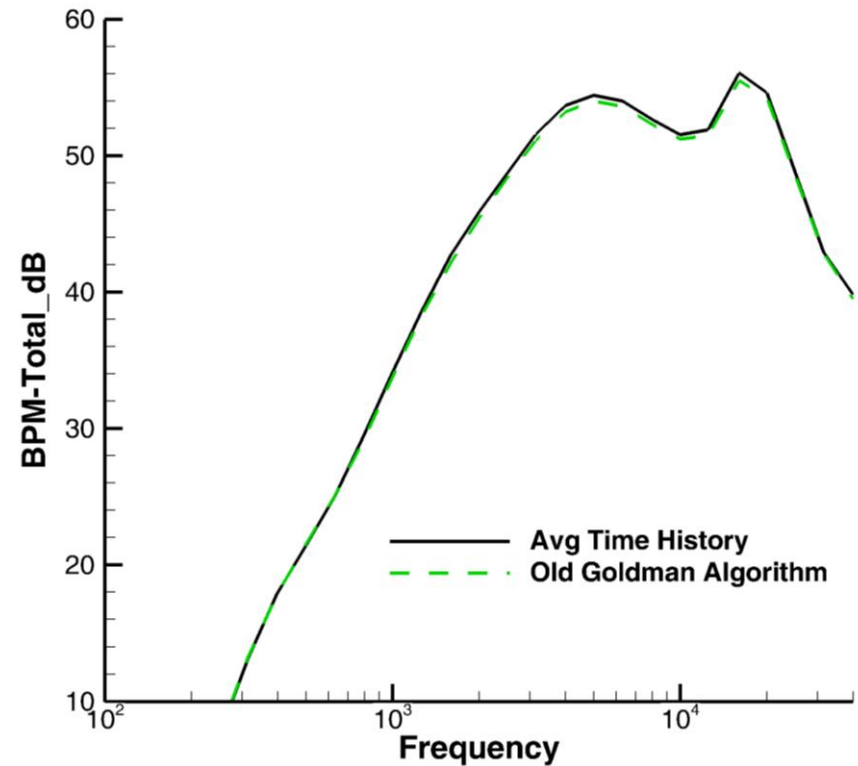


- Validation approach: Check if
 1. Time-**averaged** BPM model implemented correctly:
i.e., match BPM model predictions of other code(s)
 2. Time-**varying** BPM predictions match experimental data
- Previous validation with flight test data [3]:
modulation captured, but levels under-predicted
- Improved validation case: NASA ideally-twisted rotor
 - NASA provided time-averaged noise predictions
 - Used to check implementation (Step #1)
 - NASA provided noise measurements
 - Processing measured data to compare with time-varying PSU-WOPWOP predictions (Step #2)
 - Wind tunnel environment more controlled than outdoor flight test

[3] Z. F. T. Gan, K. S. Brentner, and E. Greenwood, 28th AIAA/CEAS Aeroacoustics Conference, 2022.

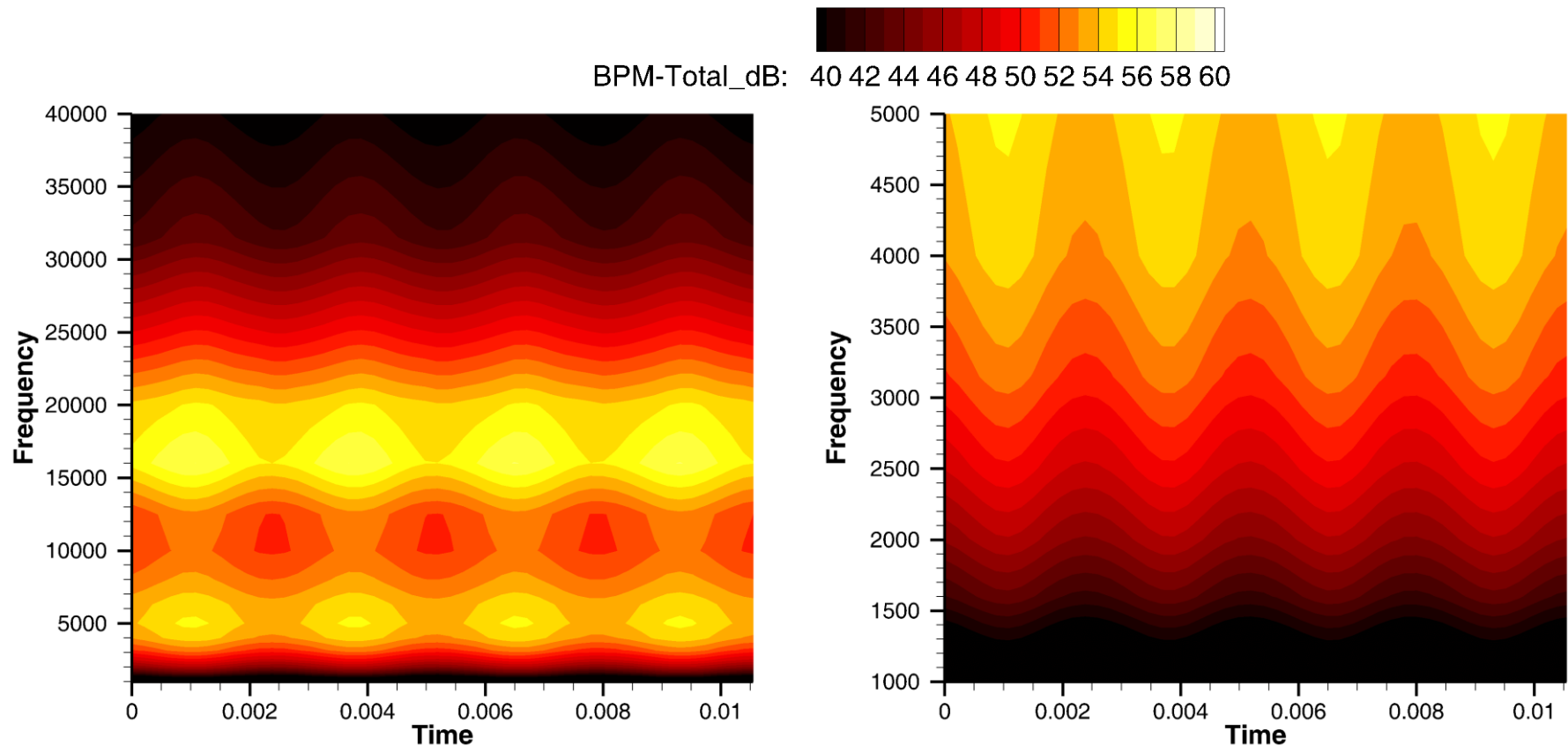
Validation – Time-averaged spectrum

- Previously validated prior to implementing time-varying broadband noise prediction framework
- After implementing time-varying broadband noise:
 - Time-averaging of spectrum time history does NOT significantly change results generated using previous PSU-WOPWOP versions



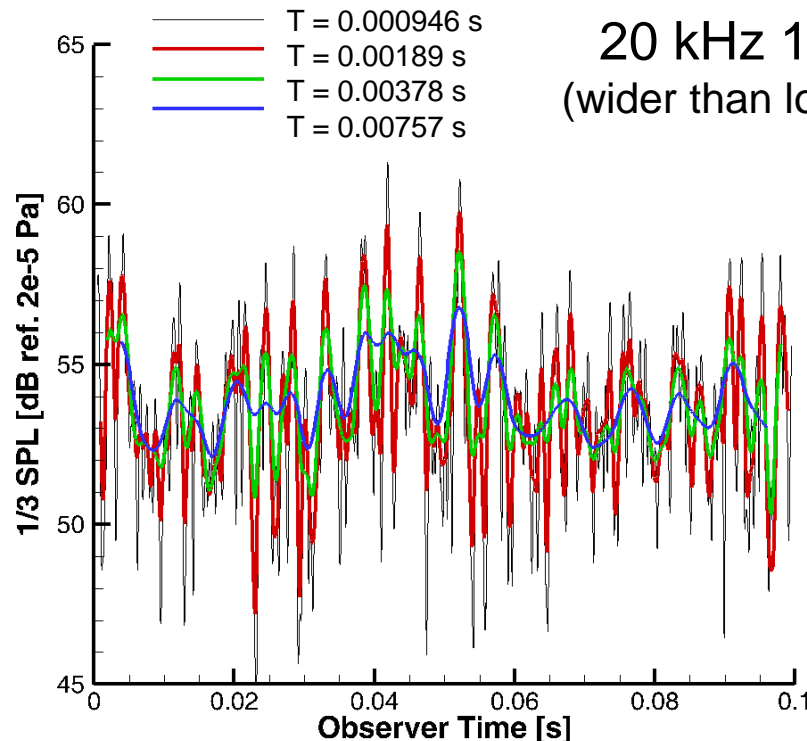
Validation – Time-varying spectrum

- Predicted time-varying broadband noise
- Will compare with experimental data, currently being processed



Validation – Spectrogram

- Processed experimental data into spectrogram
 - Modulation sensitive to chosen time window length **T**
 - Time-frequency trade-off for spectrograms:
 - Criteria: **T** \ll **BPP** (blade passage period)
 - Result: Δf \gg **BPF** (blade passage frequency)
 - If $\Delta f >$ **bandwidth**, cannot resolve frequencies below this band



Wind turbine noise studies:

- Window length $<$ 5% of BPP

Our study (BPP = 0.0027 s):

- $T = 0.000946$ s \rightarrow 0.35 BPP
- $T = 0.00189$ s \rightarrow 0.7 BPP
- $T = 0.00378$ s \rightarrow 1.4 BPP
- $T = 0.00757$ s \rightarrow 2.8 BPP

- Alternative solution to processing experimental data:
Apply cyclostationary analysis:
 - Class of statistical methods developed to study modulating signals
 - Used to study time-varying wind turbine noise:
by creating time-frequency representations (TFR)
- TFR created by cyclostationary analysis:
Offers advantages over spectrograms:
 - More mathematically correct than stationarity:
 - Spectrogram assumes spectrum constant over chosen window
 - Better time-frequency resolution:
 - Cyclostationary analysis: $\Delta f \leq \text{BPF}$
 - Spectrogram: $\Delta f \gg \text{BPF}$
- In progress: creating TFR using cyclostationary analysis

Turbulence Interaction Noise



- Motivation:
 - Geometric configurations of UAM aircraft create many opportunities for aerodynamic interactions
 - Only self-noise is modeled by BPM model
 - Broadband noise underpredicted when only self-noise included: by past Project 49 work and literature
- Upstream turbulence ingested into rotor generates broadband noise
 - Atmospheric
 - Rotor and/or airframe wake ingestion

Turbulence Interaction Noise



- Chosen model: Amiet's leading edge noise model:
time and frequency domain approaches:
 - Frequency domain approach:
 - Input: turbulence velocity spectrum
- Next steps: implement in noise prediction system
 - Integrate into existing time-varying broadband noise prediction framework used for BPM model for self-noise

- Major Accomplishments:
 - Analysis of departure maneuver for lift-plus-cruise eVTOL
 - Aircraft transitioning from hover to cruise while gaining altitude
 - Time-varying broadband noise implementation in system made more robust
 - Conducted literature review of turbulence ingestion noise models to implement in system
- Future Work:
 - Validate time-varying broadband noise predictions by processing experimental data using cyclostationary analysis
 - Implement models of broadband ingestion noise generated by aerodynamic interactions
 - Include impact of aerodynamic interactions such as BVI, BWI etc.

References



- A. Christian, J. Caston, and E. Greenwood and F. H. Schmitz, “Regarding the Perceptual Significance and Characterization of Broadband Components of Helicopter Source Noise,” Vertical Flight Society 75th Annual Forum & Technology Display, Philadelphia, Pennsylvania, May 13–16, 2019.
- Z. F. T. Gan, K. S. Brentner, and E. Greenwood and F. H. Schmitz, “Time Variation of Rotor Broadband Noise,” Vertical Flight Society 9th Biennial Autonomous VTOL Technical Meeting, Virtual, January 26–28, 2021.
- Z. F. T. Gan, K. S. Brentner, and E. Greenwood and F. H. Schmitz, “Time Variation of Helicopter Rotor Broadband Noise,” 28th AIAA/CEAS Aeroacoustics Conference, Southampton, UK, June 14-17, 2022.

Contributors

- PI: Kenneth S. Brentner, Penn State University (PSU)
- Co-PIs:
 - Eric Greenwood and Joseph F. Horn (PSU)
 - Daniel A. Wachspress and Mrunali Botre (CDI)
- Graduate Research Assistants: Ze Feng Gan and Bhaskar Mukherjee (PSU)
- Industrial Partners: Continuum Dynamics, Inc. (CDI)

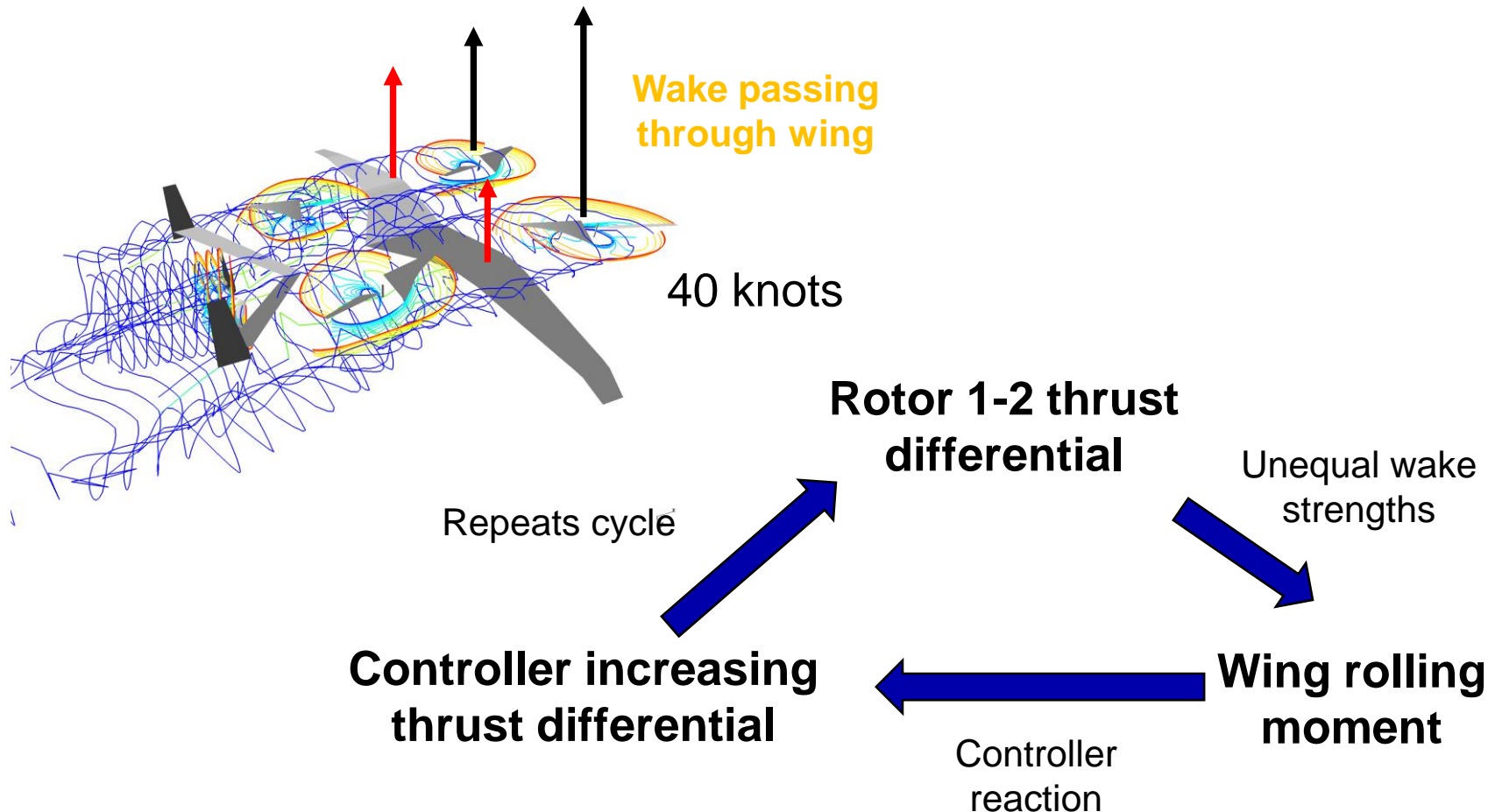
Questions?

**Extra draft slides (delete them
from final)**



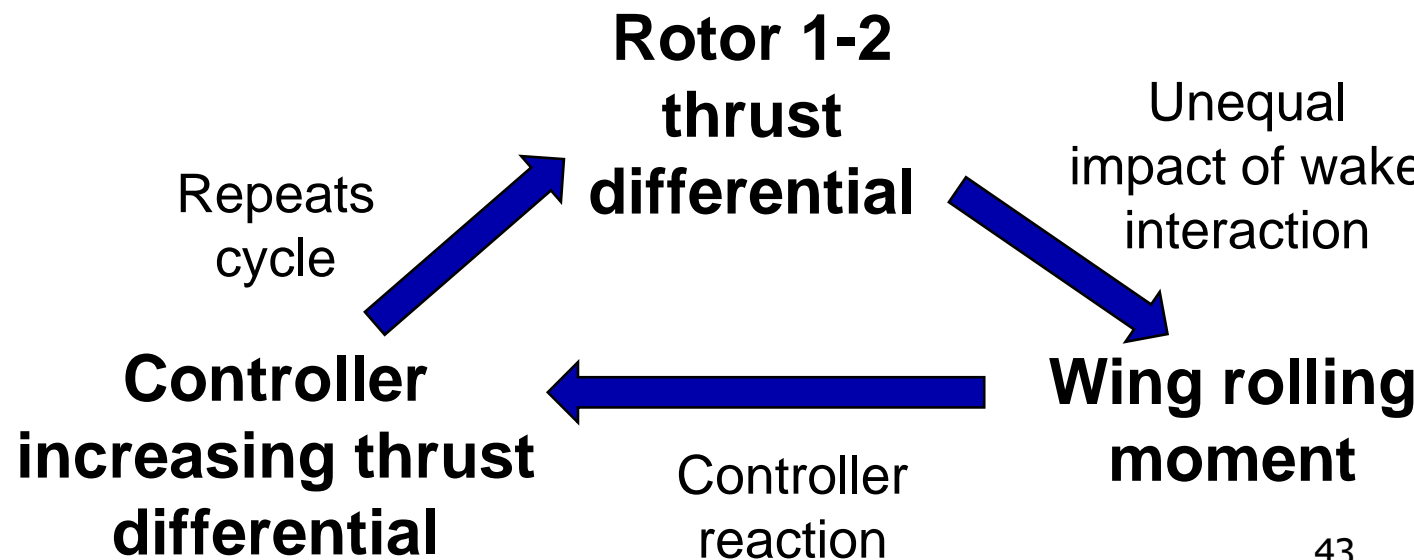
Role of interaction in dynamics

- DEPSim controls aircraft roll disturbance using the difference in thrust between rotors on each side
 - Rot 1 – Rot 2 thrust & Rot 3 – Rot 4 thrust



Role of interaction in dynamics

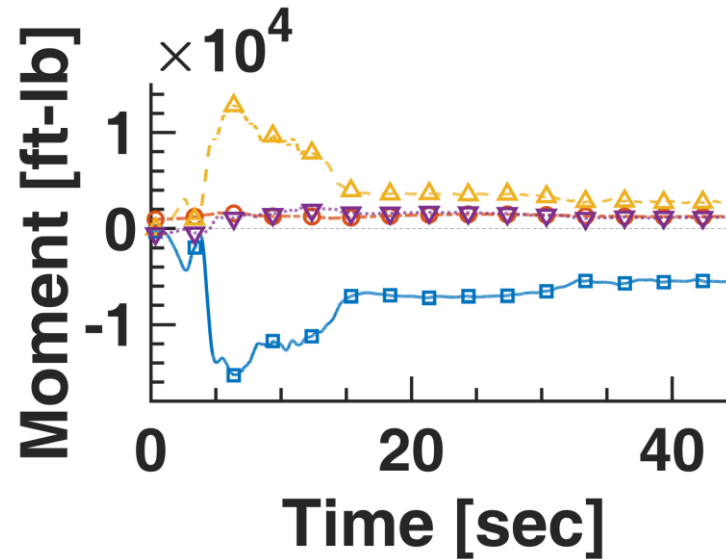
- DEPSim controls aircraft roll disturbance using the difference in thrust between rotors on each side
 - Rot 1 – Rot 2 thrust & Rot 3 – Rot 4 thrust



Rolling Moment: 70 knots

- Break moment cycle by changing how the controller compensates for rolling moment
 - Do not use rotors 1-2 thrust differential for roll rejection!
- Steady flight simulation 70 knots
 - Controller starts without knowledge of interactions
 - Interaction feedback starts around 5 seconds

■ Total Rotor Moment ⊕ Cruise Prop Moment
▲ Total Wing Moment ▼ Total Horizontal Stabilizer Moment

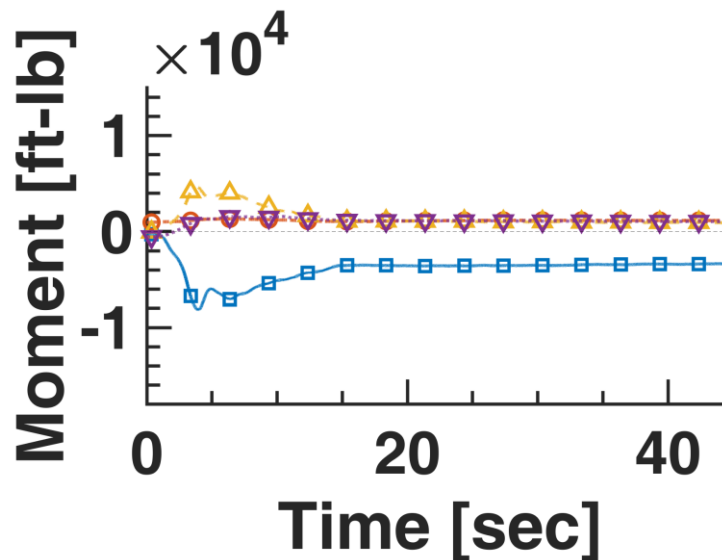


Roll moment vs Time

Rolling Moment: 70 knots

- Same steady flight simulation
- **Change in controller design**
 - Rotor 1,2 no longer involved in roll rejection
- Notice large reduction in wing and rotors moments
 - Improvement in controllability and performance
 - No significant change in noise

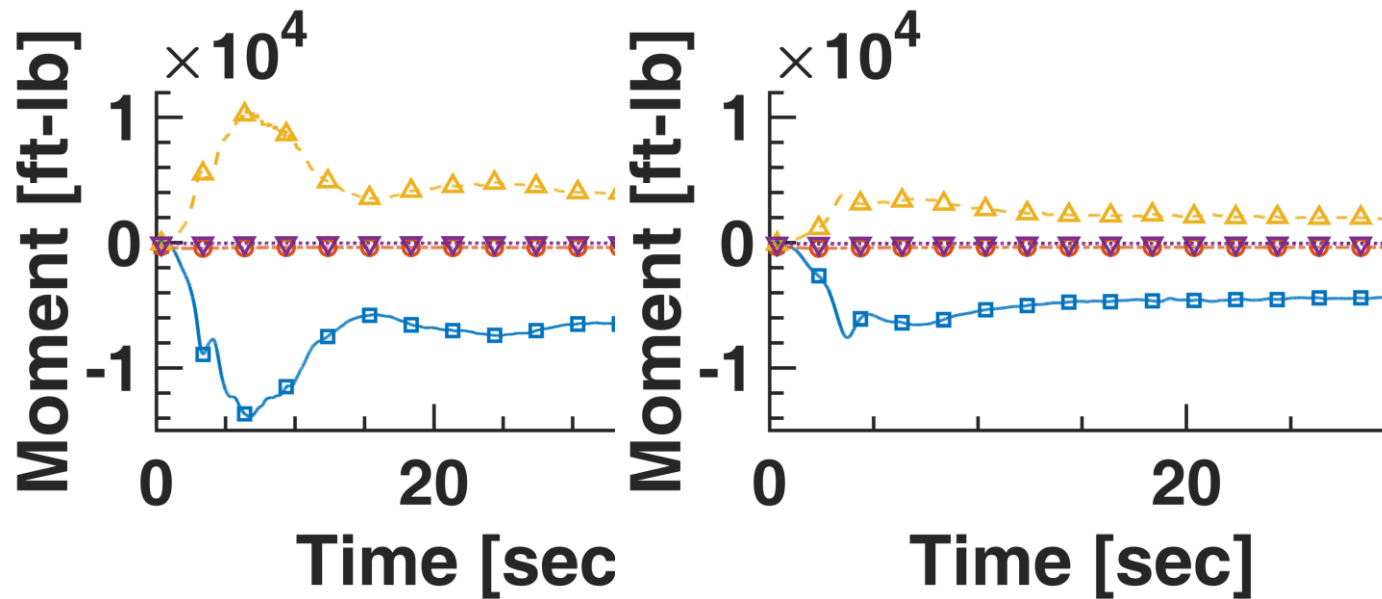
■ Total Rotor Moment ⊕ Cruise Prop Moment
▲ Total Wing Moment ▼ Total Horizontal Stabilizer Moment



Roll moment vs Time

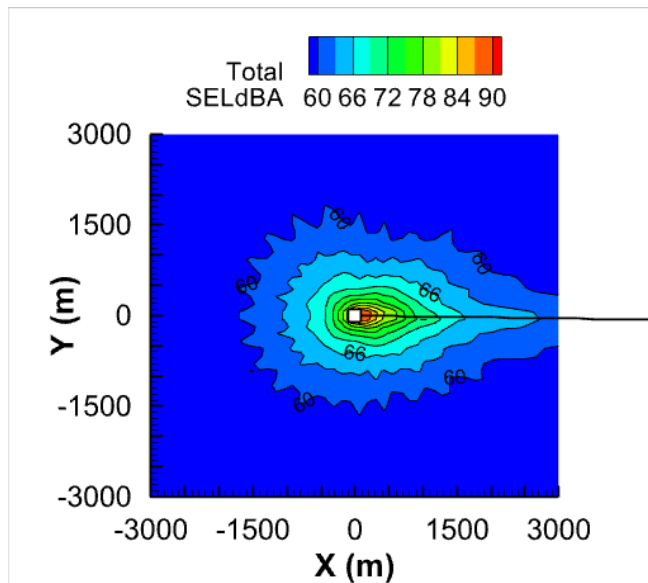
Rolling Moment: 70 knots

■ Total Rotor Moment - CHARM On ⊖ Total Rotor Moment - CHARM Off
▲ Total Wing Moment - CHARM On ▼ Total Wing Moment - CHARM Off

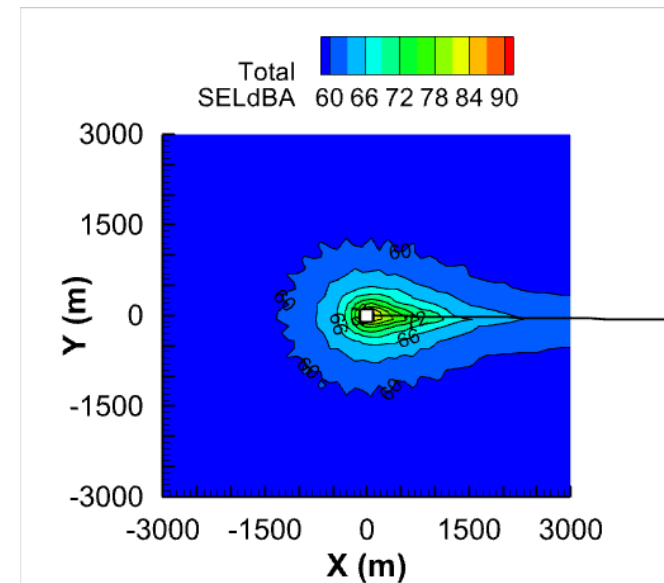


Departure maneuver: Noise

- **Level acceleration:** Lowest energy, lowest peak power
 - Lift rotor stall: 10 – 30 %
- Note difference in SEL levels when stall broadband noise is removed
 - BPM is semi-empirical and we can separate components out!



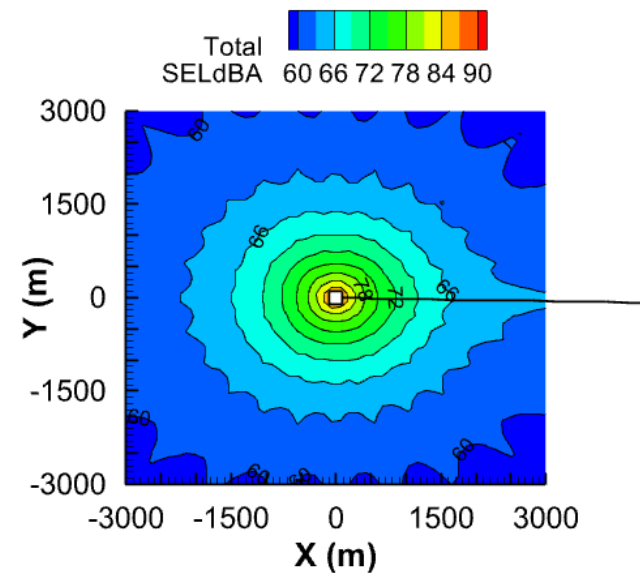
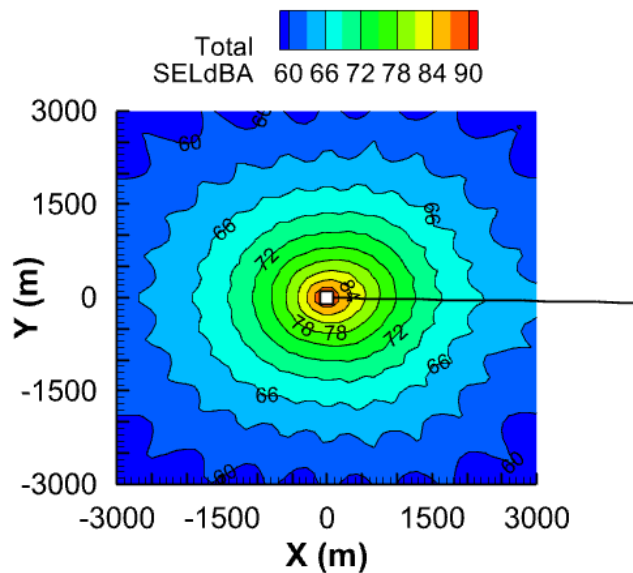
Total noise



Total noise excluding
stall from BPM

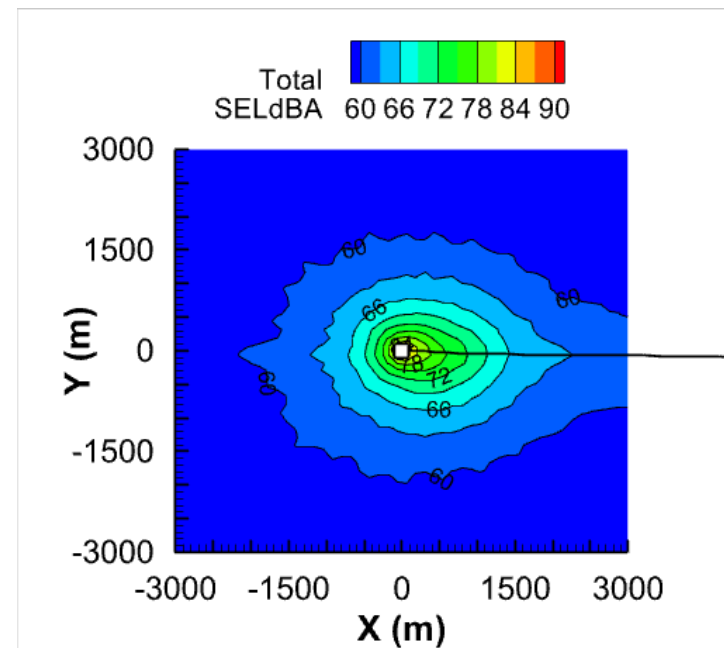
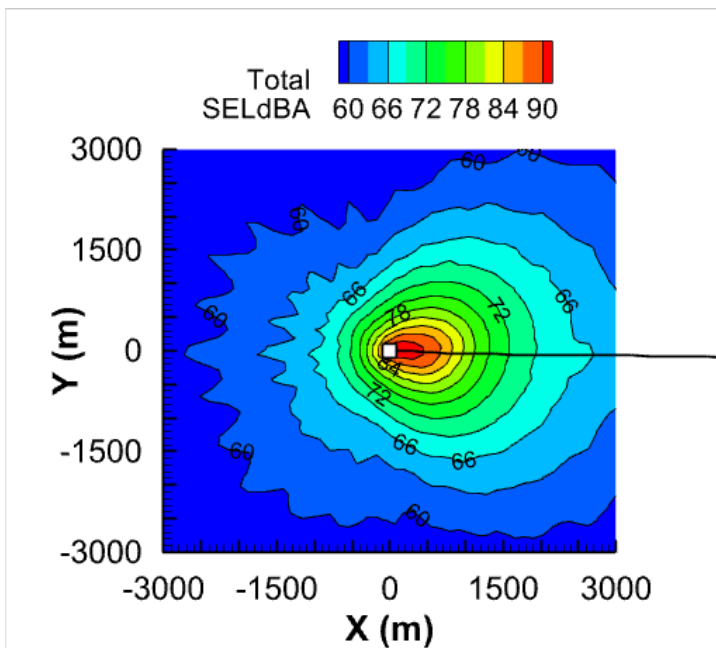
Departure maneuver: Noise

- **Axial climb:** Highest energy, second highest peak power
 - Lift rotor stall: 10 – 40 %
- Note difference in SEL levels when stall broadband noise is removed
 - **Design of blade matters!!!**



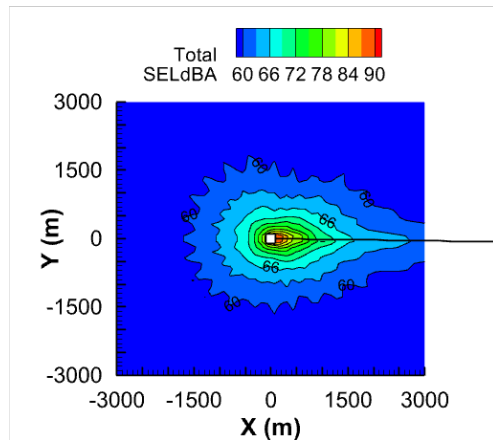
Departure maneuver: Noise

- **Continuous climb** : Second highest energy, Highest peak power
 - Lift rotor stall: 10 – 50 %
- Note difference in SEL levels when stall broadband noise is removed
 - Stall was contributing to significant noise!

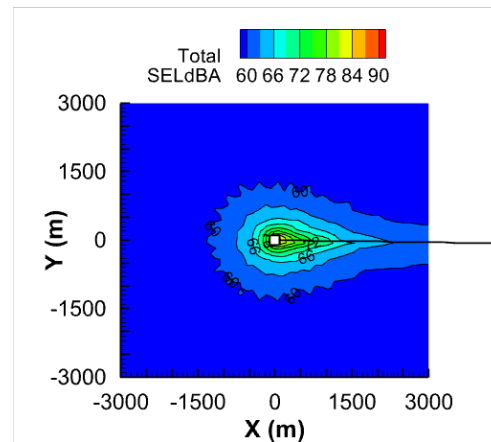


Departure maneuver: Noise

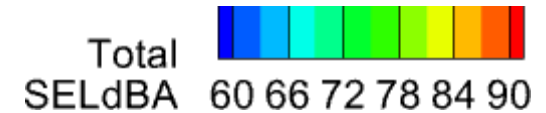
- **Level acceleration:** Lowest energy, lowest peak power
 - Lift rotor stall: 10 – 30 %
- Stall is not playing a major role in noise
 - Setpoint schedule works



Total noise

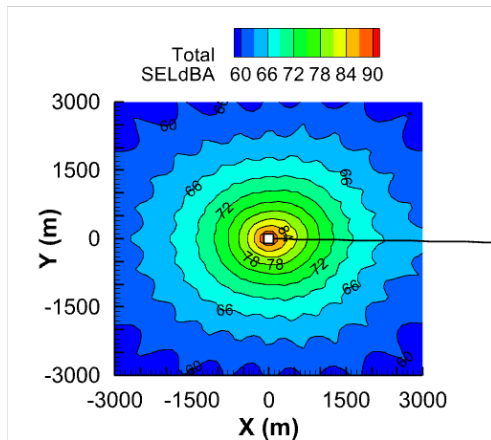


Total noise excluding stall from BPM

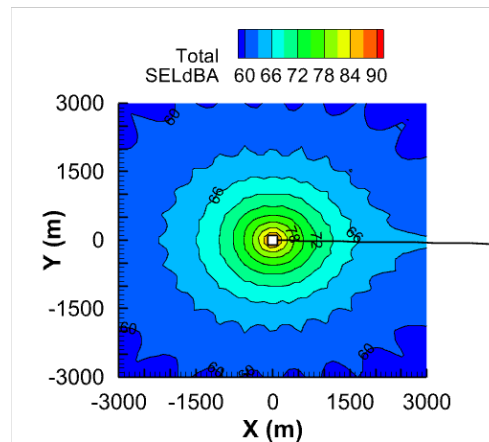


Departure maneuver: Noise

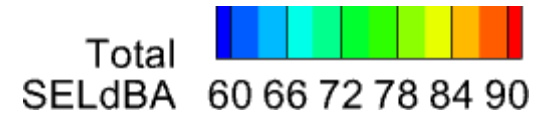
- **Level acceleration:** Lowest energy, lowest peak power
 - Lift rotor stall: 10 – 30 %
- Stall is not playing a major role in noise
 - Setpoint schedule works



Total noise

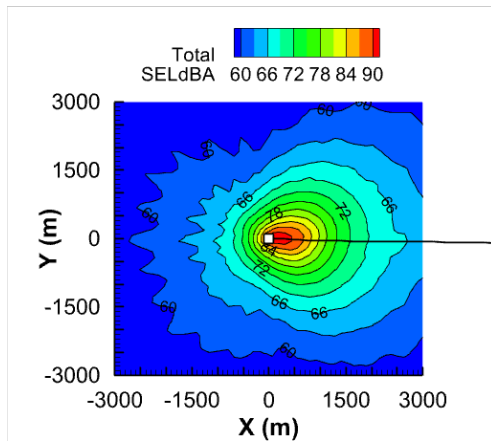


Total noise excluding stall from BPM

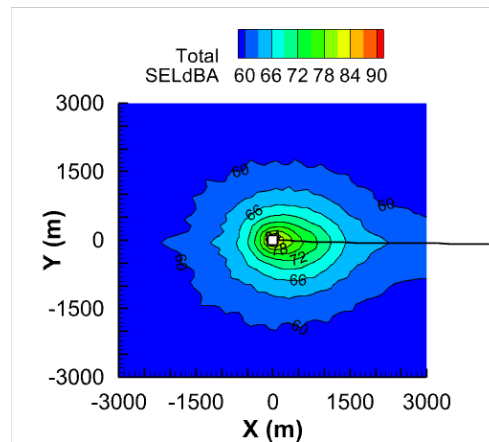


Departure maneuver: Noise

- **Level acceleration:** Lowest energy, lowest peak power
 - Lift rotor stall: 10 – 30 %
- Stall is not playing a major role in noise
 - Setpoint schedule works



Total noise



Total noise excluding stall from BPM

