

CALCULATING SECOND ORDER SENSITIVITY COEFFICIENTS FOR  
AIRPORT EMISSIONS IN THE CONTINENTAL U.S. USING CMAQ-HDDM

BY

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## Abstract

We present higher order sensitivity coefficient calculations for  $O_3$  and  $PM_{2.5}$  formation with respect to aircraft emissions in the continental United States, showing the importance of including second order sensitivity coefficients when utilizing sensitivity analyses methods for understanding the impacts of aviation emissions. We designated  $NO_X$  and VOC emissions as sensitivity parameters for  $O_3$  formation; and  $NO_X$ ,  $SO_2$ , VOC, EC, OC, and  $SO_4$  emissions as sensitivity parameters for  $PM_{2.5}$  formation. The Community Multiscale Air Quality Model (CMAQ) was used to estimate the concentrations and sensitivities of air pollutants in  $36 \times 36$  km grid cells across the continental United States. First order sensitivity coefficients were calculated for all sensitivity parameters while second order sensitivity coefficients were calculated for only  $NO_X$ , VOC, and  $SO_2$  emissions. With the inclusion of second order sensitivity coefficients we are able to show regions of chemical regime ( $NO_X$ -limited versus  $NO_X$ -inhibited) change in the case of  $O_3$  formation and areas where oxidant limiting indirect effects are important in the case of  $PM_{2.5}$  formation. Overall, we find that  $NO_X$  emissions are the largest source of nonlinear behavior exhibited in our system. This nonlinear behavior can have an impact on the tropospheric chemistry governing  $O_3$  and  $PM_{2.5}$  formation and must be considered when trying to understand how aircraft emissions may impact air quality. We present an analysis utilizing these sensitivity coefficients to estimate the emission reduction needed in five airport grid cells to bring hypothetical regions in  $PM_{2.5}$  nonattainment into attainment. Utilizing first order sensitivities, we find that 8.00, 18.41, 16.86, 7.05, and 11.77 times fewer emissions are needed at Hartsfield-Jackson Atlanta International Airport (ATL), Denver International Airport (DEN), John F. Kennedy International Airport (JFK), Los Angeles International Airport (LAX), and Chicago O'Hare International Airport (ORD), respectively to decrease concentrations of  $PM_{2.5}$  from nonattainment levels of  $14 \mu g/m^3$  to attainment levels of  $12 \mu g/m^3$ .

# Chapter 1

## Introduction

### 1.1 Aviation

The aviation sector has seen substantial growth in the past decade with air carriers flying 631 million passenger miles in the year 2015, resulting in an increase of around 11 % over the past ten years [1]. This growth is expected to continue with the Federal Aviation Administration forecasting a 2.1 % increase in U.S. carrier passenger growth each year for the next 20 years, and a 2.1 % and 3.5 % growth in system traffic in revenue passenger miles over the next 20 years for domestic travel and international travel, respectively [2].

This projected growth can place a burden on atmospheric air quality as aircraft attributable emissions become a major component of all traffic related emissions. Aircraft emissions contribute to the overall air quality through emissions of nitrogen oxides ( $\text{NO}_x$ ), sulfur oxides ( $\text{SO}_x$ ), volatile organic compounds (VOC), primary elemental carbon (PEC), primary organic carbon (POC), and primary sulfate ( $\text{PSO}_4$ ) during an aircraft's entire flight (takeoff to landing). These emissions can lead to the formation of air pollutants such as  $\text{O}_3$  and  $\text{PM}_{2.5}$ . Air pollutant formation from aviation emissions can be considered a regional problem when emissions from landing and takeoff (LTO) operations affect populations near airports, and it can be considered a global problem when emissions from higher-altitude cruise operations affect the global atmospheric chemistry. Hence, in order to understand the overall impact from aviation emissions, we need to understand the role of these emissions in forming air pollutants.

### 1.2 Particulate Matter

The U.S. Environmental Protection Agency (EPA) has designated six criteria air pollutants to be regulated under the National Ambient Air Quality Standards (NAAQS) section of the Clean Air Act [3]. These six air pollutants are particulate matter ( $\text{PM}_{10}$ ,  $\text{PM}_{2.5}$ ), ozone ( $\text{O}_3$ ), sulfur dioxide ( $\text{SO}_2$ ), nitrogen dioxide ( $\text{NO}_2$ ), carbon monoxide (CO), and lead (Pb). Regulations were devised for human health protection, however, these air pollutants have broader implications that impact the climate and chemistry of the atmosphere. In this study we will focus our efforts on PM and  $\text{O}_3$  formation from aircraft emissions.

PM can affect human health [4, 5, 6, 7, 8, 9, 10, 11], Earth's climate [12], visibility [13, 14], and climate change uncertainty through indirect radiative forcing [12, 13, 14, 15, 16, 17, 18, 19, 20, 21]. Particulate matter refers to all internally and externally mixed particles found in the atmosphere. The solid or liquid mixture can vary in composition and formation, but the main measure of particulate matter is mass concentration. Particulate matter is classified by its aerodynamic diameter and current air quality standards have distinguished mixtures associated with adverse health effects having less than  $10\mu\text{m}$  ( $\text{PM}_{10}$ ) and less than  $2.5\mu\text{m}$  ( $\text{PM}_{2.5}$ ) aerodynamic diameters. However, the degree of health impact varies amongst PM components [22, 23]. Sources for combustion-related PM include industrial combustion, transportation related combustion (including motor-vehicles, aircraft, and marine vessels), and biomass burning. PM can be directly emitted or it can be formed in the atmosphere. These distinctions are labeled as primary PM and secondary PM, respectively. NAAQS have designated annual concentrations greater than  $12\mu\text{g}/\text{m}^3$  and daily concentrations greater than  $35\mu\text{g}/\text{m}^3$  to be harmful.

### 1.3 Ozone

Like PM, Ozone ( $\text{O}_3$ ) has also been designated a standard under the NAAQS, and in 2015 it was revised to an even more stringent standard [24]. Primary and secondary concentration of  $\text{O}_3$  higher than 0.070 parts per million (ppm) averaged over an 8-hour daily period is considered harmful. Tropospheric  $\text{O}_3$  largely arises from a series of reactions initiated by sun light, involving nitrogen dioxide ( $\text{NO}_2$ ) and volatile organic compounds (VOCs). The availability of  $\text{NO}_2$  and VOCs in the lower atmosphere is largely influenced by anthropogenic sources. Nitrogen oxide (NO) emissions from mobile and stationary combustion processes react with  $\text{O}_3$  and other radicals to form  $\text{NO}_2$ , and VOCs can be directly emitted from the same combustion processes.

Other anthropogenic emissions, such as  $\text{SO}_2$ , can effect tropospheric  $\text{O}_3$  formation indirectly by affecting the tropospheric chemistry that governs the availability of  $\text{O}_3$  precursors. Even PM has recently been linked to influencing tropospheric  $\text{O}_3$  chemistry through radiative forcing feedback [25, 26, 27, 28, 29, 30, 31, 32, 33].

Impacts from  $\text{O}_3$  include environmental impacts and human health impacts.  $\text{O}_3$  can limit plant and crop growth when they are exposed to higher levels of  $\text{O}_3$  [34], and human exposure to  $\text{O}_3$  has been linked to impaired lung and cardiovascular functions [35, 36, 37].

With regards to our mobile source sector of interest contributing to combustion-related air pollution emissions,  $\text{PM}_{2.5}$  contributions from aviation are expected to increase with LTO aircraft operations increasing annual average concentrations of  $\text{PM}_{2.5}$  from 0.05% to 0.20% by 2025 [38]. An increase in aviation emissions will lead to a larger impact on health with one study on 99 U.S. airports estimating an increase in premature deaths due to aviation emissions from 75 deaths in 2005 to 460 deaths in 2025 [39]. Our study will look to understand how aviation emissions during LTO operations affect the formation of  $\text{PM}_{2.5}$  and  $\text{O}_3$ .

## Chapter 2

### Methods

#### 2.1 Air Quality Modeling

In this work we utilize an Eulerian atmospheric chemical transport model (CTM) to quantify the concentration and transport of PM,  $\text{O}_3$ , and other pollutants in a  $36 \times 36$  km grid cell resolution domain. We assume each chemical species in each grid cell to be well mixed and the model generates a concentration of each chemical species at each time step. The Community Multiscale Air Quality modeling system (CMAQ) [40], an Eulerian atmospheric CTM, has been used in this work.

Most Eulerian atmospheric CTMs calculate chemical species concentrations in each grid cell at each time step by solving the advection-diffusion-reaction equation (Eq. 2.1).

$$\frac{dC_i}{dt} = -\nabla(\vec{u} C_i) + \nabla(\vec{K} C_i) + R_i + E_i \quad (2.1)$$

In the advection-diffusion-reaction equation,  $C_i$  is the concentration of a chemical species denoted with subscript  $i$ ,  $\vec{u}$  is the wind field,  $\vec{K}$  is the turbulence diffusivity tensor,  $R_i$  is the reaction rate of species  $i$ , and  $E_i$  is the emission rate of chemical species  $i$ . This ordinary differential equation describes the change in concentration of any chemical species in the model over time.

#### 2.2 Decoupled Direct Method

Various sensitivity analyses in the atmospheric CTM framework are used for guiding policy and environmental scenarios. One simple and commonly used method is the Brute Force method which relies on a subtractive or finite-difference analysis approach. For this analysis, at least two model simulations are run with one case having some input parameter varied and the other case is left unchanged. The difference between the two cases describes the effect of the varied input parameter. This can be done for as many scenarios as needed with each scenario requiring two model simulations.

The advantage of the Brute Force (BF) method is its simplicity. Most other sensitivity analyses methods are compared with the BF method. Limitations of the BF method include the computational cost required for performing multiple scenarios and the often noisy output concentrations that may arise when input parameters are varied by small amounts. We use a sensitivity analysis method that can handle multiple scenarios and reduce the noise from small variations. This method is known as the Decoupled Direct Method in Three Dimensions (DDM-3D) [41, 42, 43].

While BF methods are performed with output from model simulations, DDM-3D is performed within the model at each time step. Derivatives are taken at each time step which calculate the change in concentration of a chemical species with respect to some change in an input parameter. In the CMAQ DDM-3D framework, input parameters that can be varied include initial conditions, boundary conditions, emissions, and reaction rates. Output from DDM-3D is in the form of sensitivity coefficients which express the derivatives taken at each time step (Eq. 2.2).

$$S_{i,j}^1 = \frac{\partial C_i}{\partial E_j} \quad (2.2)$$

Equation 2.2 shows the form of the sensitivity coefficient  $S$  as calculated in the DDM-3D analysis. The superscript <sup>1</sup> denotes a first order change to some chemical species  $C_i$  with respect to a varying input parameter  $E_j$ . In our case we will only concern ourselves with varying emission input parameters, as denoted by  $E$ . These sensitivity coefficients will propagate through our model simulation and CMAQ DDM-3D provides the solution to a modified advection-diffusion-reaction equation (Eq. 2.3).

$$\frac{\partial S_{i,j}^1}{\partial t} = -\nabla(\vec{u} S_{i,j}^1) + \nabla(\vec{K} S_{i,j}^1) + J_i S_j^1 + E_i \quad (2.3)$$

The modified advection-diffusion-reaction equation is in terms of the first order sensitivity coefficients  $S_{i,j}^1$  and  $J_i$  denotes the  $i$ -th row of a Jacobian matrix of reaction rates. First order sensitivity coefficients describe linear changes in concentrations with respect to changing emissions. In our case of air pollutants attributable to aviation emissions, we need to be concerned with air pollutant species that may not be linearly dependent on aviation emissions. The chemistry surrounding tropospheric PM<sub>2.5</sub> and O<sub>3</sub> formation is far more complicated than what can be expressed with only first order changes. Hence, we will extend our DDM-3D analysis framework to what is known as higher order decoupled direct method in three dimensions (HDDM-3D) in order to calculate second order sensitivity coefficients. In doing so, we hope to capture more of the chemistry related to PM<sub>2.5</sub> and O<sub>3</sub> formation from aviation emissions to understand how aviation impacts air pollution.

## 2.3 Higher Order Decoupled Direct Method

Here we will outline two types of second order sensitivity coefficients. Full derivations of HDDM-3D can be found in Hakami et. al 2003 [44] and Zhang et. al 2012 [45] with the latter paying special attention to the treatment of Secondary Organic Aerosols (SOA) within the HDDM-3D framework.

One type of second order sensitivity coefficient is calculated by simply taking the second derivative of Eq. 2.2 with respect to parameter  $E_j$ .

$$S_{i,j}^2 = \frac{\partial^2 C_i}{\partial E_j^2} \quad (2.4)$$

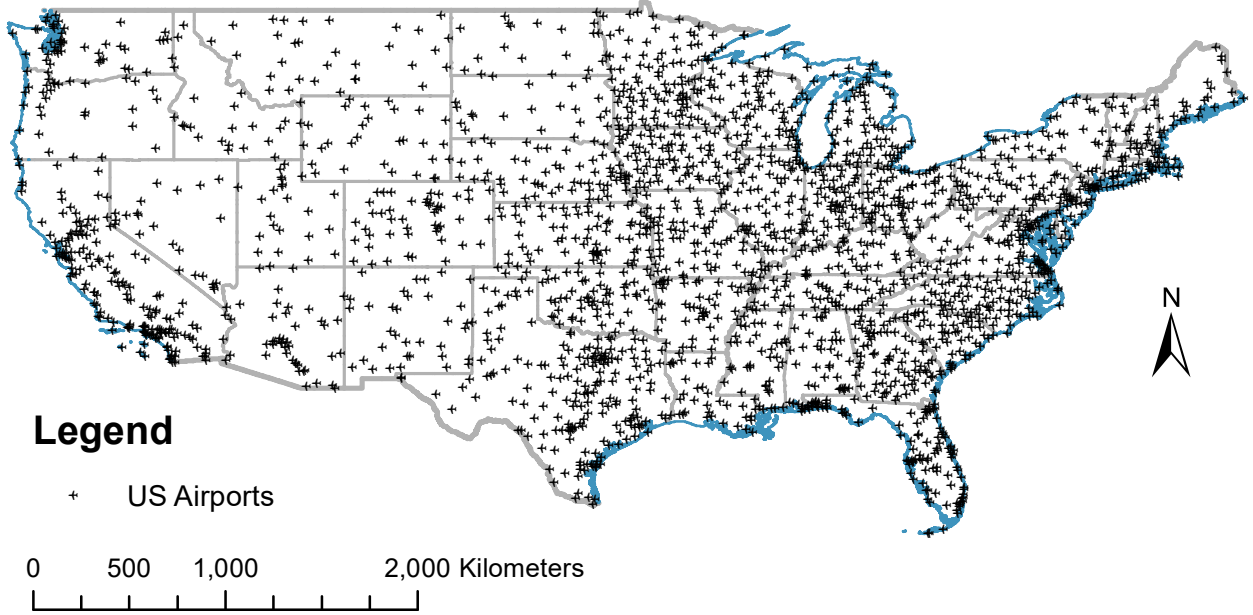
Eq. 2.4 is the second order change of a species  $C_i$  with respect to some varying input parameter  $E_j$ . The second type of second order sensitivity coefficient relies on the separability of the partial differential equations that govern atmospheric CTMs. HDDM-3D can also calculate second order cross-sensitivity coefficients that describe the change in concentration of chemical species  $C_i$  with respect to *two* varying input parameters  $E_j$  and  $E_k$  (Eq. 2.5).

$$S_{i,j,k}^2 = \frac{\partial^2 C_i}{\partial E_j \partial E_k} \quad (2.5)$$

The resulting advection-diffusion-reaction equation with second order cross-sensitivity coefficients can be written in a simplified form as:

$$\begin{aligned} \frac{\partial S_{i,j,k}^2}{\partial t} = & -\nabla(\vec{u} S_{i,j,k}^2) + \nabla(\vec{K} \nabla S_{i,j,k}^2) + \\ & \vec{J}_i \vec{S}_{j,k}^2 + f(C_i, S_{i,j}^1, S_{i,k}^1, \vec{u}, \vec{K}, R_i, E_i). \end{aligned} \quad (2.6)$$

In Eq. 2.6, superscripts <sup>1</sup> and <sup>2</sup> denote first order and second order sensitivity coefficients, respectively.  $\vec{J}_i$  is  $i$ -th row of a Jacobian matrix of reaction rates and  $\vec{S}_{j,k}^2$  is a vector of second order sensitivity coefficients. For brevity, the function  $f$  contains the relationships between the concentration of species  $i$ , first order sensitivity coefficients with respect to parameters  $j$  and  $k$ , the wind and turbulence diffusivity tensors, and the reaction and emission rates of species  $i$ . In this general form, the equation can be applied to any varying



**Figure 2.1:** Locations of the 2,106 active airports considered in our CONUS domain.

input parameter, not just changes to emissions. Details of this function  $f$  can be found in Eq. (9) in Hakami et al. 2003 [44].

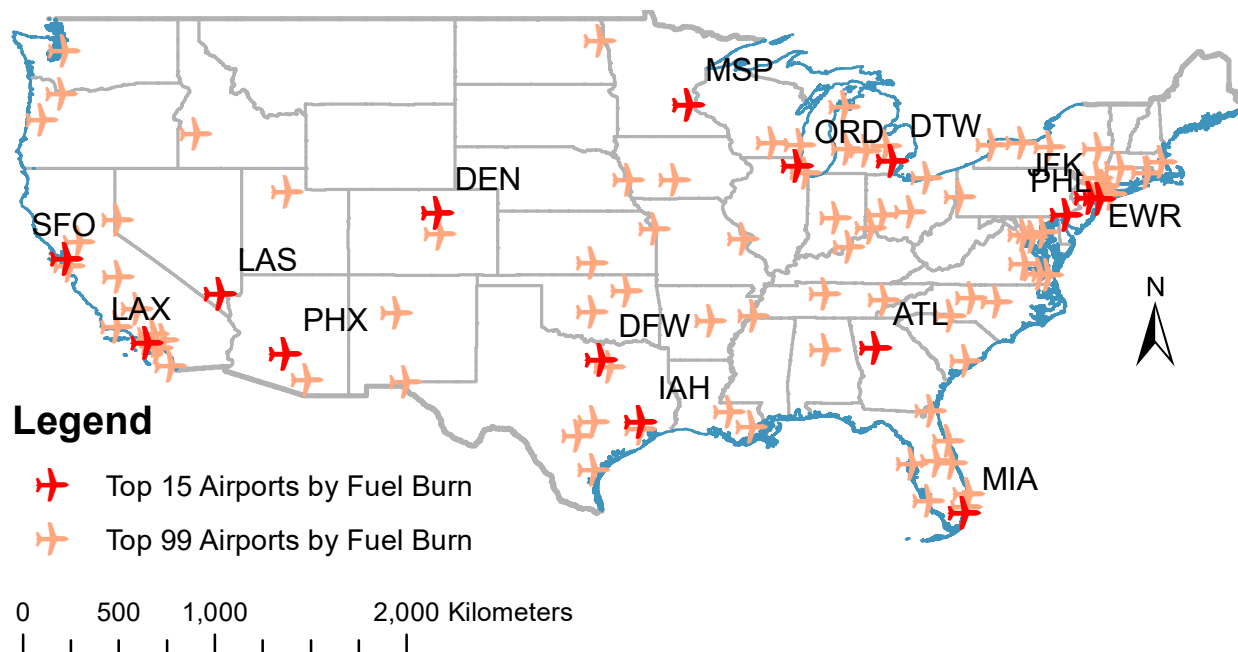
For our study, six precursor emissions that are responsible for the formation of  $\text{PM}_{2.5}$  and  $\text{O}_3$  are chosen as sensitivity parameters for first order DDM-3D analyses. Three gas phase species; nitrogen oxides ( $\text{NO}_x$ ), sulfur dioxide ( $\text{SO}_2$ ), volatile organic compounds (VOC), and three particle phase species; primary elemental carbon (PEC), primary organic carbon (POC), and primary sulfate ( $\text{PSO}_4$ ) are directly emitted from aircrafts and they all can lead to the formation of  $\text{PM}_{2.5}$  and  $\text{O}_3$  in the atmosphere. We limit our sensitivity parameters for second order HDDM-3D analyses to the three gas phases species since these species are responsible for secondary formation of pollutants in the atmosphere. Table 2.1 shows the species included in the CMAQ simulation for our precursor emissions.

## 2.4 Domain

Our domain consists of the continental United States (CONUS) with a  $148 \times 112$  grid of  $36\text{km} \times 36\text{km}$  resolution. We utilize the FAA’s Aviation Emission Design Tool (AEDT) [46] for constructing aircraft flight segments from the 2,106 active airports in the United States. Figure 2.1 shows all of the airports considered in our domain. We consider only landing and takeoff flight segments; that is all flight segments below 3,000 ft. By considering only LTO operations, we are focusing our efforts on effects from aircraft emissions at a regional level. And although our model simulation is performed with 34 vertical layers into the atmosphere, we will consider DDM-generated sensitivities within the model at only the surface layer for the purpose of understanding health impacts in populations located near airports.

LTO segments are processed into gridded emission rate files using AEDTProc [47]. Background emission rates, defined to be all non-aviation related emissions, from EPA’s National Emissions Inventories (NEI-2005) [48] are processed into gridded emission rate files using the Sparse Matrix Operator Kernel Emissions (SMOKE) [49]. Meteorology data for 2005 is from the Weather Research and Forecasting model (WRF) [50], with outputs downscaled from NASA’s Modern-Era Retrospective Analysis for Research and Applications data (MERRA) [51]. 2005 Boundary conditions are derived from global CAM-chem simulations [52]. Simulations are performed for the months of January and July in 2005 with a 10 day spin up for each month. January and July are chosen to approximately represent winter and summer characteristics seen during each half of the year. Future work will expand the temporal domain over the entire year.

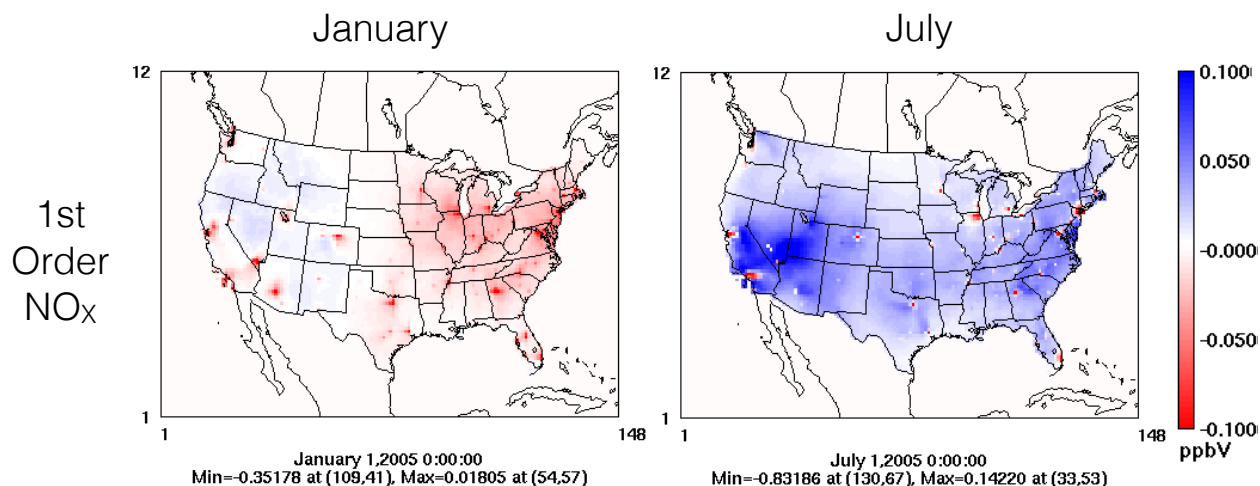




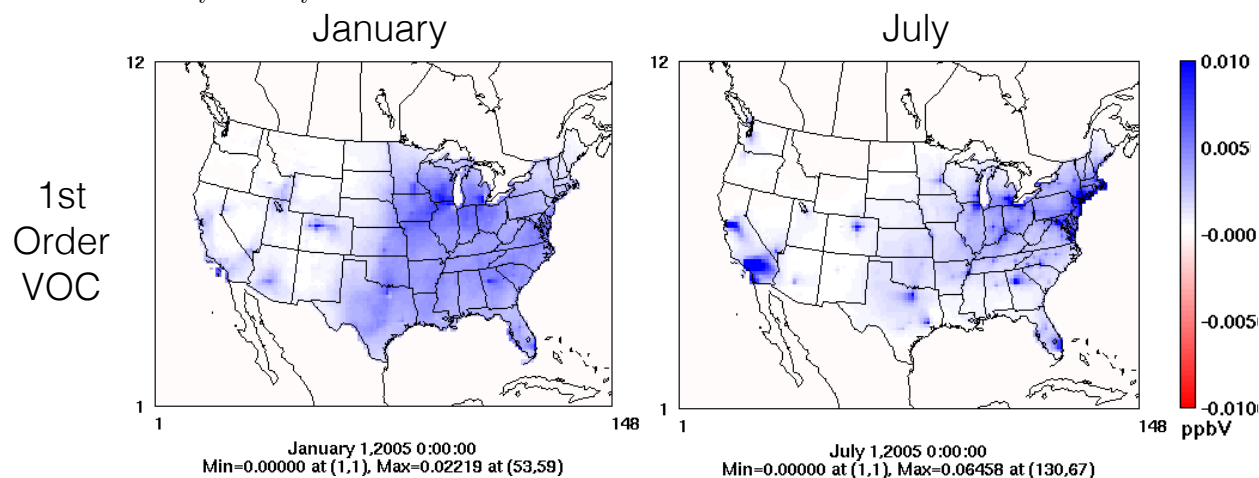
**Figure 2.2:** Locations of the top 99 US airports responsible for the largest total fuel burn considered in our CONUS domain. This is for purely illustrative purposes.

Group	Model Species	Name
NO <sub>x</sub>	NO	Nitric oxide
	NO <sub>2</sub>	Nitrogen dioxide
	HONO	Nitrous acid
EC	PEC	Primary elemental carbon
OC	POC	Primary organic carbon
SO <sub>4</sub>	PSO <sub>4</sub>	Primary sulfate
SO <sub>2</sub>	SO <sub>2</sub>	Sulfur dioxide
VOC	ALD2	Acetaldehyde
	ALDX	Ethene
	ETHA	Ethane
	ETOH	Ethanol
	FORM	Formaldehyde
	IOLE	Internal olefin bond
	MEOH	Methanol
	OLE	Terminal olefin bond
	TOL	Toluene-like
	XYL	Xylene-like

**Table 2.1:** Sensitivity parameters as defined in the model



**Figure 3.1:** First order sensitivity calculations of  $O_3$  concentration (in ppbV) with respect to  $NO_x$  emissions for the months of January and July.



**Figure 3.2:** First order sensitivity calculations of  $O_3$  concentration (in ppbV) with respect to VOC emissions for the months of January and July.

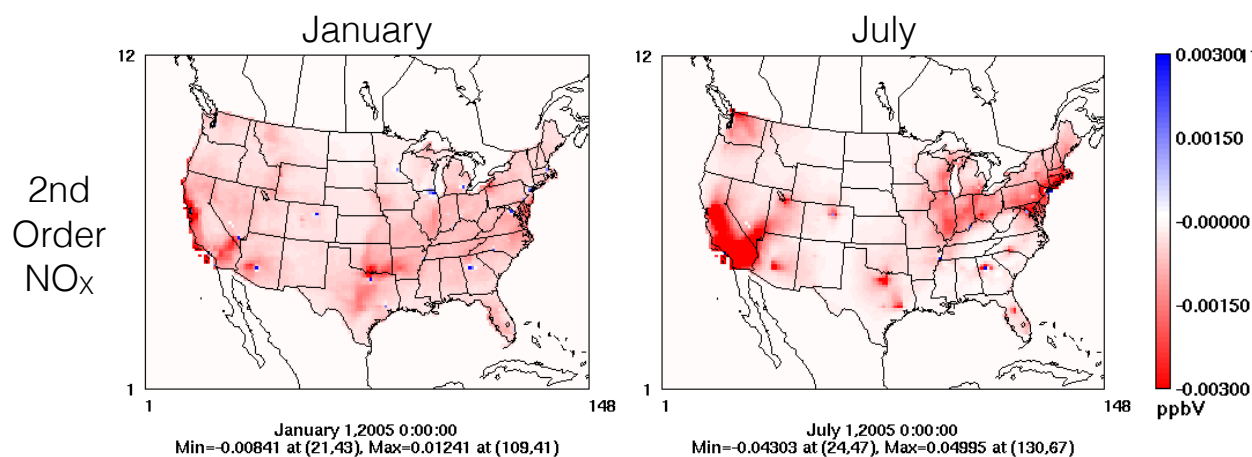
## Chapter 3

### Results

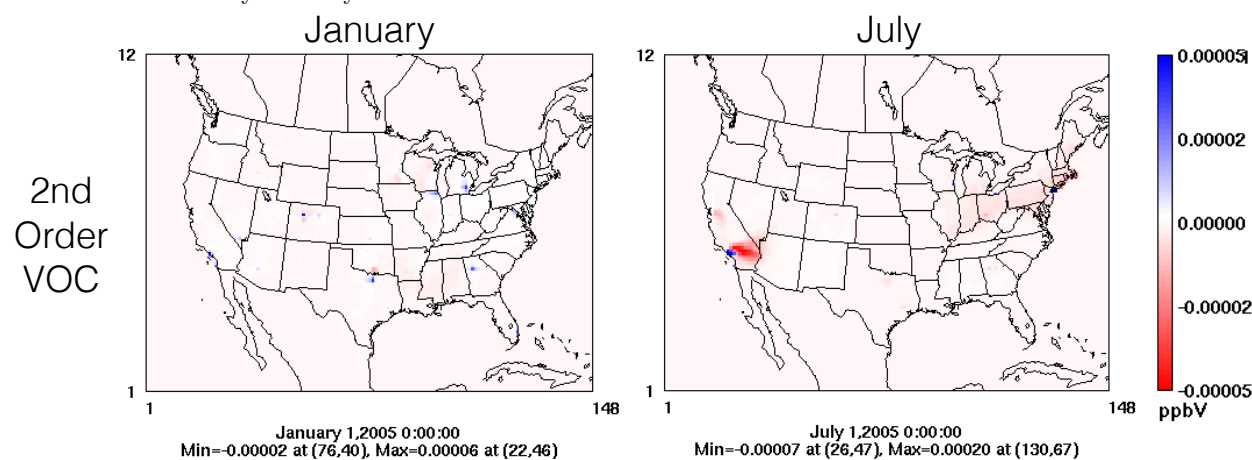
#### 3.1 $O_3$ First Order Response

We begin with calculating first order sensitivity coefficients as a way to estimate where nonlinearity, or second order changes in concentration, is important in our domain. Beginning with  $O_3$  concentration sensitivities to our aircraft precursor emissions, we can look at  $O_3$  first order sensitivities to  $NO_x$  (90% NO, 9%  $NO_2$ , and 1% HONO for aviation emissions) and VOC aviation emissions.

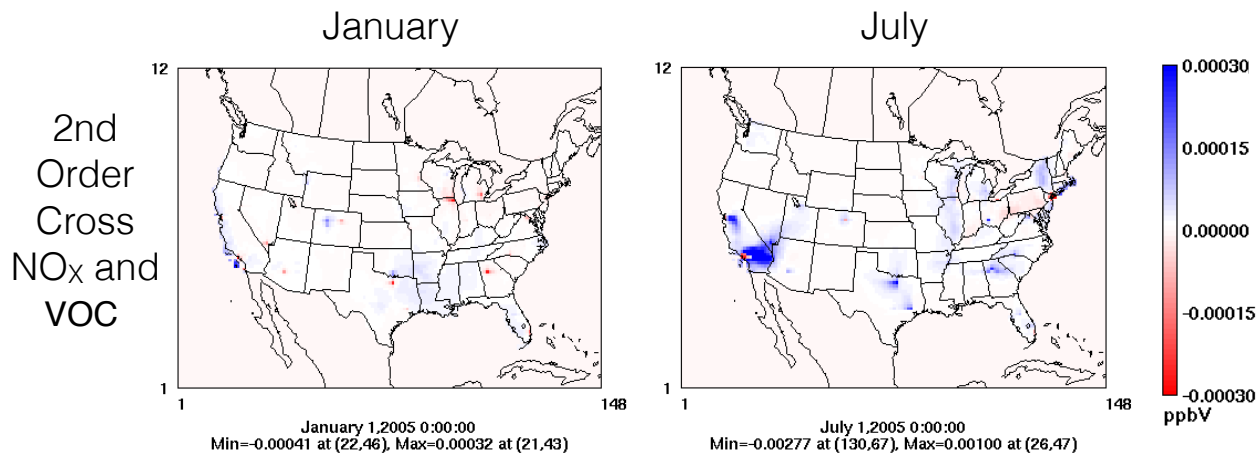
Figures 3.1 and 3.2 show the DDM first order sensitivity coefficients for  $O_3$  sensitivity to  $NO_x$  and VOC emissions, respectively. Seasonal differences indicate a nonlinear concentration response to  $NO_x$  emissions with an indication of a possible chemical regime change in July. Chemical regime refers to whether an area is considered to be  $NO_x$ -limited or  $NO_x$ -inhibited (VOC limited). Tropospheric  $O_3$  formation is predicated by the availability of  $NO_x$  and VOCs in a given region reacting with the OH radical [53]. And since  $NO_x$  and VOCs compete for available OH in the atmosphere, the  $O_3$  formation pathways can vary based on the



**Figure 3.3:** Second order sensitivity calculations of  $O_3$  concentration (in ppbV) with respect to  $NO_x$  emissions for the months of January and July.



**Figure 3.4:** Second order sensitivity calculations of  $O_3$  concentration (in ppbV) with respect to  $NO_x$  emissions for the months of January and July.



**Figure 3.5:** Second order sensitivity calculations of  $O_3$  concentration (in ppbV) with respect to  $NO_x$  and VOC emissions for the months of January and July.

emissions of VOCs or  $\text{NO}_x$  in a region. Regions with high  $\text{NO}_x$  emissions leading to  $\text{O}_3$  formation are deemed  $\text{NO}_x$ -inhibited (VOC-limited) and are often highly localized to urban regions. Regions where available VOCs are comparable to available  $\text{NO}_x$  are deemed  $\text{NO}_x$ -limited and tend to categorize most suburban to rural areas. However, it is not the case that simply reducing emissions of  $\text{NO}_x$  in a  $\text{NO}_x$ -inhibited regime or reducing VOCs in a  $\text{NO}_x$ -limited regime will lead to reductions of  $\text{O}_3$ . Due to the nonlinearity of  $\text{O}_3$  production pathways, emission control strategies for reducing  $\text{O}_3$  differ based on which chemical regime one may be in. EKMA diagrams were one of the first analyses to show how  $\text{O}_3$  concentrations change with reductions of  $\text{NO}_x$  and VOCs in  $\text{NO}_x$ -inhibited and  $\text{NO}_x$ -limited regimes [54]. They rely on knowing the  $\text{O}_3$  concentrations for varying amounts of  $\text{NO}_x$  and VOCs in a given region. This makes them hard to replicate from a modeling perspective since each varied amount of  $\text{NO}_x$  and VOCs require an additional modeling simulation. DDM and HDDM is advantageous in this respect [55, 56, 44] since their outputs allow for a comprehensive understanding of how  $\text{O}_3$  concentrations change with respect to varying  $\text{NO}_x$  and VOC emissions across our domain. Chemical regimes will be indicated by how  $\text{O}_3$  either increases or decreases with respect to increasing or decreasing  $\text{NO}_x$  and VOC emissions.

Negative first order sensitivity coefficients with respect to  $\text{NO}_x$  emissions in the immediate proximity of the major U.S. airports indicate a  $\text{NO}_x$ -inhibited regime for January and July. However, regions of positive first order sensitivity coefficients (Downwind of SFO, LAX, ATL) in the month of July indicate a shift to a  $\text{NO}_x$ -limited regime. First order sensitivity to VOC emissions exhibits a largely linear behavior with positive first order sensitivity coefficients across the entire domain. Hence, using first order DDM analyses, we can estimate where nonlinear changes in  $\text{O}_3$  become important. In our case, this nonlinearity represents a chemical regime change downwind of larger urban airports.

### 3.2 $\text{O}_3$ Second Order Response

Figures 3.3 and 3.4 show the HDDM second order sensitivity coefficients for  $\text{O}_3$  sensitivity to  $\text{NO}_x$  and VOC, respectively. As we had anticipated from the first order responses to VOC emissions,  $\text{O}_3$  concentration response is mostly linear and second order sensitivity coefficients are one to two orders in magnitude smaller than first order sensitivity coefficients. Nonlinearity can be seen in the immediate vicinity of Los Angeles and downwind of LAX in the month of July.

Lastly, we can examine the second order cross-sensitivity of  $\text{O}_3$  concentration response to both  $\text{NO}_x$  and VOC emissions. Figure 3.5 shows the HDDM second order cross-sensitivity coefficients for  $\text{O}_3$  sensitivity to  $\text{NO}_x$  and VOC emissions in our domain. Cross-sensitivity responses are inherently more complicated to conceptualize, with the concentration response now determined by variations of two types of emissions. This becomes important for describing the formation of  $\text{O}_3$  in terms of which chemical regime,  $\text{NO}_x$ -limited or  $\text{NO}_x$ -inhibited, one may be concerned with. In a  $\text{NO}_x$ -limited regime,  $\text{O}_3$  production (denoted as  $P_{\text{O}_3}$ ) is linearly dependent on NO (Eq. 3.1).

$$P_{\text{O}_3} \sim \text{NO} \quad (3.1)$$

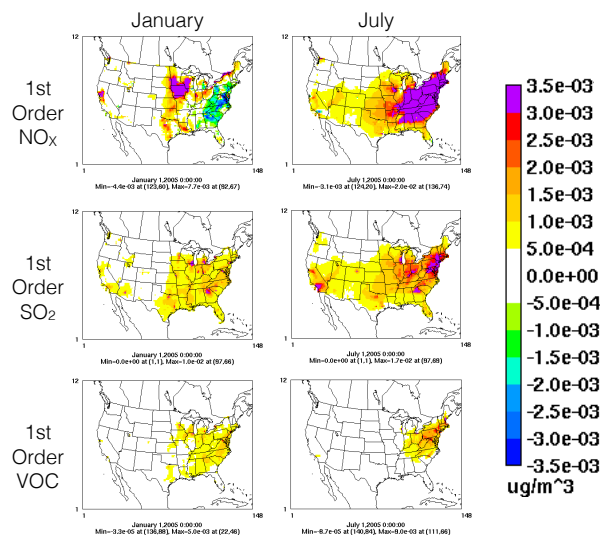
In a  $\text{NO}_x$ -inhibited regime,  $\text{O}_3$  formation is linearly dependent on VOCs and inversely dependent on  $\text{NO}_2$ .

$$P_{\text{O}_3} \sim \frac{\text{VOC}}{\text{NO}_2} \quad (3.2)$$

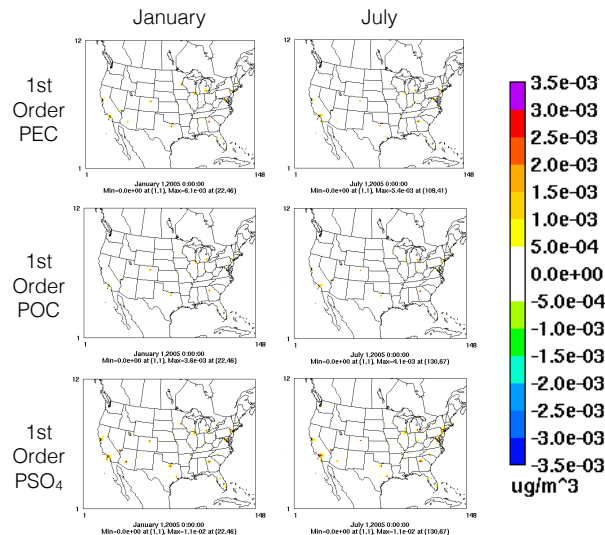
In our case, we can clearly distinguish  $\text{NO}_x$ -limited and  $\text{NO}_x$ -inhibited regimes by looking at cross-sensitivity coefficients. If we consider LAX and the region downwind, our second order cross-sensitivity coefficients are negative in the immediate area surrounding LAX and positive downwind. And since we know our first order sensitivity coefficients to  $\text{NO}_x$  to be one to two orders of magnitude higher than our sensitivity coefficients to VOC, the region immediately surrounding LAX is  $\text{NO}_x$ -inhibited while the rural downwind area is  $\text{NO}_x$ -limited. The transition between regimes can be seen with our nonzero second order sensitivity coefficients.  $\text{NO}_x$  availability governs  $\text{O}_3$  formation and  $\text{NO}_x$  emissions from aircrafts are responsible for the highest degree of nonlinear behavior when considering  $\text{O}_3$  precursor emissions from aircrafts.

### 3.3 $PM_{2.5}$ First Order Response

Figure 3.6 and 3.7 show  $PM_{2.5}$  first order sensitivity coefficients with respect to our six varying precursor emissions:  $NO_X$ ,  $SO_2$ , VOC, PEC, POC, and  $PSO_4$ . Although we have emissions from 2,106 airports in our domain, significant impacts (values on the order of  $10^{-3}$ ) are seen at only major airports (Fig. 2.2). This can be seen by looking at  $PM_{2.5}$  sensitivities to our particle phase species, PEC, POC, or  $PSO_4$  where the impact on PM formation from these precursors are highly localized to the points of emission; in this case, the major airports (Fig. 3.7). This PM formation can be considered primary while  $PM_{2.5}$  sensitivities to  $NO_X$ ,  $SO_2$ , and VOC are significant up to several hundred kilometers from the emission source indicative of secondary PM formation.



**Figure 3.6:** First order sensitivity calculations of  $PM_{2.5}$  concentration (in  $\mu g/m^3$ ) with respect to  $NO_X$ ,  $SO_2$ , and VOC emissions for the months of January and July.



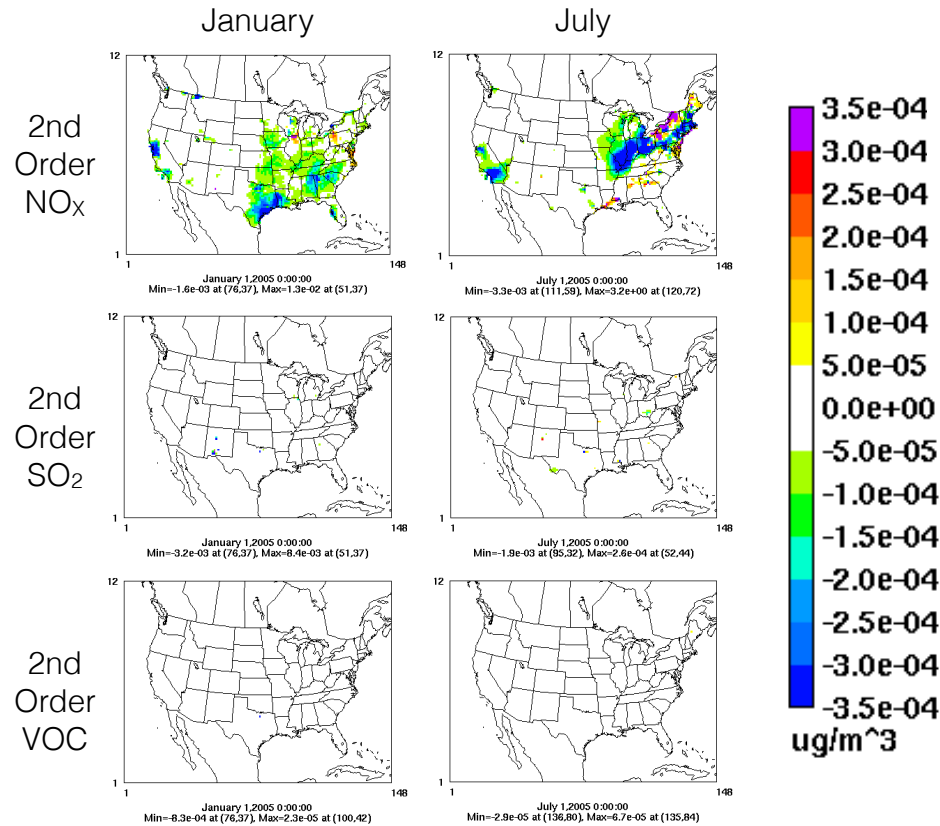
**Figure 3.7:** First order sensitivity calculations of  $PM_{2.5}$  concentration (in  $\mu g/m^3$ ) with respect to PEC, POC, and  $PSO_4$  emissions for the months of January and July.

Seasonal differences indicate larger first order sensitivity coefficients across all precursor emissions in the month of July than January. The only significant negative first order sensitivities are seen with respect to  $NO_X$  emissions. In January, large areas of negative first order sensitivity coefficients are seen in the southeast U.S. stretching up the coast. In July, this same region becomes positive and the few areas that exhibit negative first order coefficients are Los Angeles and downwind of LAX, the Miami area, Chicago, and San Francisco.

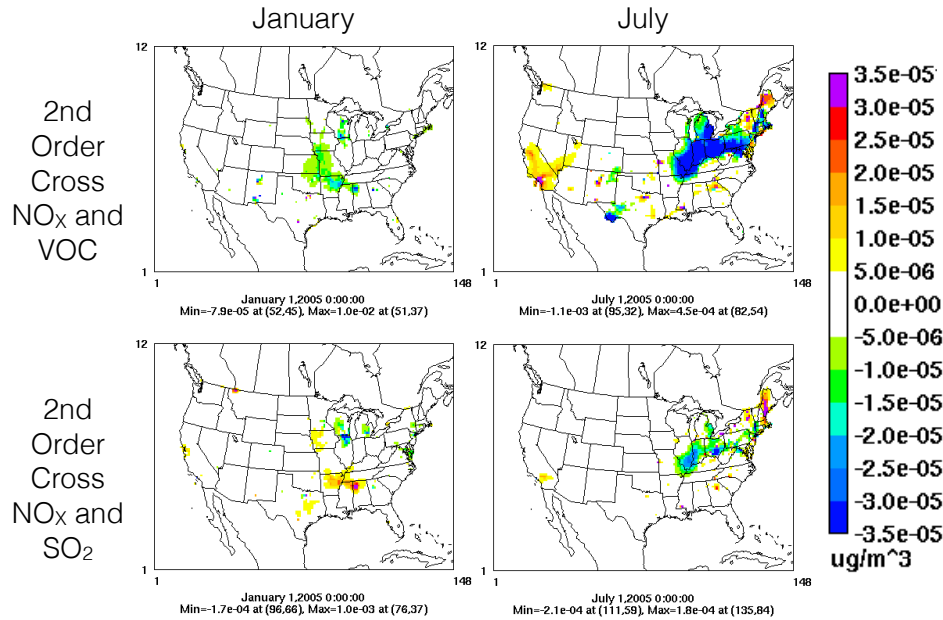
### 3.4 $PM_{2.5}$ Second Order Response

Figure 3.8 shows the second order sensitivity coefficients for  $PM_{2.5}$  with respect to  $NO_X$ ,  $SO_2$ , and VOC emissions. We can see the most second order impact of  $PM_{2.5}$  with respect to  $NO_X$  emissions. And although aircrafts are not direct emitters of ammonia ( $NH_3$ ), availability of  $NH_3$  can affect the partitioning of secondarily formed nitrate into particle phase owing to the overall  $PM_{2.5}$  formation [57]. One work has studied how the availability of  $NH_3$  impacts aviation-attributable emissions [38].  $NH_3$  availability affecting the partitioning of secondarily formed nitrate into particle phase is evident by looking at  $NO_X$  nonlinear sensitivities in regions where background  $NH_3$  is available to affect nitrate formation, such as the southeast U.S. and the midwest U.S. during winter months.

Similar to  $NH_3$  availability affecting secondary nitrate formation, oxidant availability can affect secondary sulfate and nitrate formation. This arises through indirect effects often attributable to sensitivities to two or more precursors. HDDM becomes a perfect method for capturing these indirect effects by calculating sensitivities to multiple inputs. Figure 3.9 shows the second order cross-sensitivity coefficients for  $PM_{2.5}$  with respect to  $NO_X$  and  $SO_2$  and  $NO_X$  and VOC emissions. Availability of oxidants such as  $HO_X$  radicals



**Figure 3.8:** Second order sensitivity calculations of  $PM_{2.5}$  concentration (in  $\mu g/m^3$ ) with respect to  $NO_x$ ,  $SO_2$ , and VOC emissions for the month of January and July.



**Figure 3.9:** Second order cross-sensitivity calculations of  $PM_{2.5}$  concentration (in  $\mu g/m^3$ ) with respect to  $NO_x$  and  $SO_2$  emissions, and  $NO_x$  and VOC emissions for the month of January and July.

(HO<sub>x</sub> = OH+peroxy) and O<sub>3</sub> leading to oxidation of SO<sub>2</sub> can limit sulfate formation and add to the overall PM<sub>2.5</sub>. If SO<sub>2</sub> emissions are reduced in this oxidant limiting case, more oxidants are available to convert SO<sub>2</sub> from other sources [57]. The oxidant limiting case is important for aircraft emissions because we are concerned with changes in SO<sub>2</sub> emissions that are small when compared to other SO<sub>2</sub> sources seen on the east coast. Oxidant limiting effects are also temperature dependent and we can see this with our second order cross-sensitivity coefficients for NO<sub>x</sub> and SO<sub>2</sub> emissions for January and July. With lower temperatures in January, more nitric acid (HNO<sub>3</sub>) can dissolve into water which means NO<sub>x</sub> aircraft emission reductions also reduces the aqueous phase acidity. This then increases sulfate formation as more SO<sub>2</sub> dissolves and then oxidizes in the aqueous phase [57]. With higher temperatures in July, oxidant availability is limited by reducing NO<sub>x</sub> emissions, leading to less oxidation of SO<sub>2</sub> and sulfate formation beyond sulfate reduction through SO<sub>2</sub> emissions reduction alone. We can see these seasonal differences in figure 3.9 with July showing a large area of negative cross sensitivities to NO<sub>x</sub> and SO<sub>2</sub> emissions in the Ohio valley stretching over to the east coast and an area of positive cross sensitivities to NO<sub>x</sub> and SO<sub>2</sub> emissions downwind of LAX where SO<sub>2</sub> background emissions are considerably less.

Although the effects are smaller, oxidant availability altered by reductions in NO<sub>x</sub> emissions can also effect secondary organic aerosols formed through oxidation of VOC emissions. We can see this nonlinear behavior in figure 3.9 for PM<sub>2.5</sub> cross sensitivities to NO<sub>x</sub> and VOC aircraft emissions. Therefore, NO<sub>x</sub> emissions are responsible for the largest amount of nonlinear behavior.

## Chapter 4

### Attainment Analyses

#### 4.1 Emission Reductions

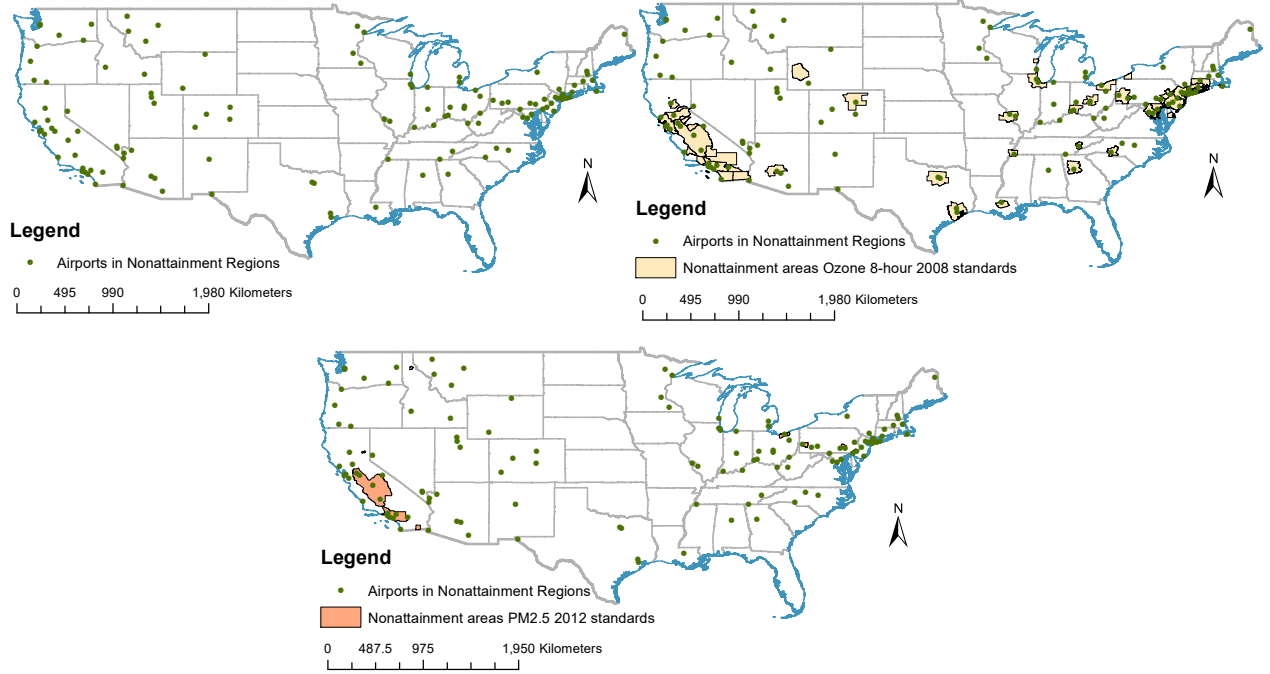
The true power of these sensitivity coefficients and the decoupled direct method in general, is its ability to estimate changes in pollutant concentrations with respect to emission reductions by only performing one model simulation. This allows for a quick and accurate way to understand how emission reductions will impact air pollutant concentrations. First and second order sensitivity coefficients can be used in simple Taylor series approximations to estimate some change in pollutant concentration,  $C_i$ , with respect to some change in emissions,  $\Delta\epsilon_j$  (Eq. 4.1) [44].

$$C_i(\Delta\epsilon_j) = C_i(0) + \Delta\epsilon_j S_{i,j}^1(0) + \frac{\Delta\epsilon_j^2}{2} S_{i,j}^2(0) \quad (4.1)$$

130 airports in the United States are currently located in areas designated as being in nonattainment of the EPA's NAAQ standards [59]. Figure 4.1 shows the locations of these 130 airports (4 located in Alaska are not shown). The airports located in regions of nonattainment of these standards pose a risk to public health by contributing to the amount of air pollutants in the region. And as aviation continues to grow as an emission sector, aviation-related health impacts will affect areas already in nonattainment. We can use DDM-3D analyses to look at the effects from individual airports. First order sensitivity coefficients were calculated for emissions from five individual airports: Chicago O'Hare International Airport (ORD), Hartsfield-Jackson Atlanta International Airport (ATL), Denver International Airport (DEN), Los Angeles International Airport (LAX), and John F. Kennedy International Airport (JFK). Table 4.1 shows the first order sensitivity coefficients for each precursor emission species. Second order sensitivity coefficients were calculated as well with table 4.2 showing second order sensitivity coefficients for all gas phase species of interest, and table 4.3 showing second order sensitivity order cross-sensitivity coefficients to NO<sub>x</sub> and SO<sub>2</sub> emissions and NO<sub>x</sub> and VOC emissions. These coefficients are values calculated at each of the airport's home grid cell, referring to impacts that would be seen within that grid cell. Hence, these coefficients can vary for regions surrounding the airport's grid cell and need to be considered when considering large populations that may be downwind of airports where the coefficient may represent secondary chemistry and meteorological impacts.

We can perform a Taylor series expansion with these sensitivity coefficients to estimate the amount of emission reductions needed to bring a region that is in nonattainment of PM<sub>2.5</sub> standards into attainment. If we imagine the region immediately surrounding Chicago O'Hare airport (ORD's home grid cell) to be in nonattainment with a concentration of PM<sub>2.5</sub> of 14  $\mu\text{g}/\text{m}^3$ , we can estimate the amount of emission





**Figure 4.1:** Locations of the 130 airports in regions designated as being in nonattainment by the EPA [58]

reductions needed for a decrease of  $2\mu\text{g}/\text{m}^3$ . Sensitivities in January are assumed to be the same for six months of the year and sensitivities in July are assumed to be the same for the other six months of the year. Using only first order sensitivity coefficients to our precursor emissions and Eq. 4.1, we would need to decrease emissions by 11.77 times in the Chicago O'Hare airport grid cell to decrease the concentration of  $\text{PM}_{2.5}$  by  $2\mu\text{g}/\text{m}^3$ . We expect larger effects to be seen by including second order sensitivity coefficients for  $\text{O}_3$  reductions and  $\text{PM}_{2.5}$  reductions in airports like Los Angeles International where second order coefficients are all negative for gas phase species. Table 4.4 shows the emission reductions needed to decrease  $\text{PM}_{2.5}$  by  $2\mu\text{g}/\text{m}^3$  for each of our five airports.

Equations 4.2 through 4.4 show how the emission amounts were calculated for our individual airports' sensitivity coefficients. We show the first order calculations with respect to our precursor emissions. Equation 4.2 shows the amount of emission reduction needed,  $\Delta\epsilon$ , to bring a region into attainment where  $C_{\text{PM}_{2.5}}(\Delta\epsilon) = 2\mu\text{g}/\text{m}^3$  when we only consider first order sensitivities to our precursor emissions,  $S_{\text{PM}_{2.5}}^1$ . Equation 4.4 shows the approximate yearly first or second (denoted with boldface superscripts <sup>1,2</sup>, while normal expressions raised to a power are not boldfaced) sensitivity coefficients with values from tables 4.1 and 4.2. Future work will utilize equation 4.3. This is the same calculation but it now includes the second order term in the Taylor series expansion which takes into account second order sensitivities.

$$C_{\text{PM}_{2.5}}(\Delta\epsilon) = \Delta\epsilon S_{\text{PM}_{2.5}}^1 \quad (4.2)$$

$$C_{\text{PM}_{2.5}}(\Delta\epsilon) = \Delta\epsilon S_{\text{PM}_{2.5}}^1 + \frac{\Delta\epsilon^2}{2} S_{\text{PM}_{2.5}}^2 \quad (4.3)$$

$$\begin{aligned} S_{\text{PM}_{2.5}}^{1,2} = & 6[S_{\text{PM}_{2.5},\text{NO}_x}^{1,2} + S_{\text{PM}_{2.5},\text{SO}_2}^{1,2} + S_{\text{PM}_{2.5},\text{VOC}}^{1,2} + S_{\text{PM}_{2.5},\text{POC}}^{1,2} + S_{\text{PM}_{2.5},\text{PEC}}^{1,2} + S_{\text{PM}_{2.5},\text{PSO}_4}^{1,2}]_{\text{JAN}} \\ & + 6[S_{\text{PM}_{2.5},\text{NO}_x}^{1,2} + S_{\text{PM}_{2.5},\text{SO}_2}^{1,2} + S_{\text{PM}_{2.5},\text{VOC}}^{1,2} + S_{\text{PM}_{2.5},\text{POC}}^{1,2} + S_{\text{PM}_{2.5},\text{PEC}}^{1,2} + S_{\text{PM}_{2.5},\text{PSO}_4}^{1,2}]_{\text{JUL}} \end{aligned} \quad (4.4)$$



	ORD		ATL		DEN		LAX		JFK	
	January	July	January	July	January	July	January	July	January	July
O <sub>3</sub> to NO <sub>x</sub>	-0.219	-0.315	-0.344	-0.361	-0.238	-0.227	-0.192	-0.617	-0.214	-0.827*
O <sub>3</sub> to VOC	0.006	0.010	0.005	0.018	0.003	0.014	0.006	0.019	0.001*	0.055
PM <sub>2.5</sub> to NO <sub>x</sub>	$4.626 \times 10^{-5*}$	-0.003	-0.003	-0.002*	-0.001	-0.002	0.002	-0.003	-0.001	-0.014
PM <sub>2.5</sub> to SO <sub>2</sub>	0.010	0.002	0.009	0.007	$3.940 \times 10^{-4*}$	0.002	0.002	0.003*	0.002	0.006
PM <sub>2.5</sub> to VOC	0.002	$2.773 \times 10^{-4}$	0.001*	$4.580 \times 10^{-4}$	0.001	$2.118 \times 10^{-4}$	0.005	0.002	0.001	0.003
PM <sub>2.5</sub> to PEC	0.004	0.002	0.004	0.005	0.003	0.002	0.006	0.005	0.001	0.004
PM <sub>2.5</sub> to POC	0.002	0.001	0.002	0.003	0.003	0.002	0.003	0.003	0.001	0.004
PM <sub>2.5</sub> to PSO <sub>4</sub>	0.005	0.003	0.005	0.008	0.004	0.003	0.011	0.009	0.002	0.010

**Table 4.1:** First order sensitivity coefficients of O<sub>3</sub> (ppb) and PM<sub>2.5</sub> ( $\mu\text{g}/\text{m}^3$ ) at each airport's home cell. \* Respective maximum or minimum not located in airport home grid cell

	ORD		ATL		DEN		LAX		JFK	
	January	July	January	July	January	July	January	July	January	July
O <sub>3</sub> to NO <sub>x</sub>	0.008	0.002	0.013	0.014	0.009	0.001	0.006	0.017	0.004	0.047
O <sub>3</sub> to VOC	$2.341 \times 10^{-5}$	$4.949 \times 10^{-6}$	$3.279 \times 10^{-5}$	$9.873 \times 10^{-6}$	$1.005 \times 10^{-5}$	$8.885 \times 10^{-6}$	$5.414 \times 10^{-5}$	$1.567 \times 10^{-4}$	$5.079 \times 10^{-6}$	$1.677 \times 10^{-4}$
PM <sub>2.5</sub> to NO <sub>x</sub>	$1.287 \times 10^{-4}$	$5.609 \times 10^{-5}$	$2.417 \times 10^{-5}$	$1.037 \times 10^{-4}$	$1.009 \times 10^{-5}$	$-1.857 \times 10^{-5}$	$-1.071 \times 10^{-4}$	$-2.018 \times 10^{-4}$	$2.134 \times 10^{-4}$	$1.169 \times 10^{-3}$
PM <sub>2.5</sub> to SO <sub>2</sub>	$-1.623 \times 10^{-4}$	$-8.514 \times 10^{-7}$	$-7.167 \times 10^{-5}$	$-2.714 \times 10^{-5}$	$-1.133 \times 10^{-7}$	$-4.943 \times 10^{-8}$	$-2.502 \times 10^{-7}$	$-7.939 \times 10^{-7}$	$-2.027 \times 10^{-5}$	$-2.995 \times 10^{-5}$
PM <sub>2.5</sub> to VOC	$-2.475 \times 10^{-5}$	$-1.460 \times 10^{-7}$	$-3.239 \times 10^{-6}$	$-8.227 \times 10^{-7}$	$-1.677 \times 10^{-6}$	$-2.789 \times 10^{-7}$	$4.654 \times 10^{-6}$	$1.573 \times 10^{-6}$	$-1.751 \times 10^{-6}$	$-2.479 \times 10^{-6}$

**Table 4.2:** Second order sensitivity coefficients of O<sub>3</sub> (ppb) and PM<sub>2.5</sub> ( $\mu\text{g}/\text{m}^3$ ) at each airport's home cell.

	ORD		ATL		DEN		LAX		JFK	
	January	July	January	July	January	July	January	July	January	July
O <sub>3</sub> to NO <sub>x</sub> and VOC	$-2.179 \times 10^{-4}$	$-1.619 \times 10^{-5}$	$-2.329 \times 10^{-4}$	$3.010 \times 10^{-5}$	$-8.713 \times 10^{-5}$	$-8.476 \times 10^{-5}$	$-3.658 \times 10^{-4}$	$-0.001$	$-4.325 \times 10^{-5}$	$-0.002$
PM <sub>2.5</sub> to NO <sub>x</sub> and SO <sub>2</sub>	$-9.282 \times 10^{-6}$	$-2.378 \times 10^{-5}$	$-3.461 \times 10^{-5}$	$-2.581 \times 10^{-5}$	$-4.518 \times 10^{-6}$	$-1.631 \times 10^{-5}$	$-1.531 \times 10^{-5}$	$-5.495 \times 10^{-5}$	$-9.706 \times 10^{-6}$	$-1.087 \times 10^{-4}$
PM <sub>2.5</sub> to NO <sub>x</sub> and VOC	$-3.040 \times 10^{-5}$	$7.438 \times 10^{-7}$	$-2.084 \times 10^{-5}$	$-1.051 \times 10^{-6}$	$-1.169 \times 10^{-5}$	$1.113 \times 10^{-6}$	$-4.583 \times 10^{-5}$	$-3.087 \times 10^{-5}$	$-2.435 \times 10^{-5}$	$-1.193 \times 10^{-4}$

**Table 4.3:** Second order cross-sensitivity coefficients of O<sub>3</sub> (ppb) and PM<sub>2.5</sub> ( $\mu\text{g}/\text{m}^3$ ) at each airport's home cell.

$\Delta\epsilon$	ORD	ATL	DEN	LAX	JFK
First order	11.77	8.00	18.41	7.05	16.86
All precursors					

**Table 4.4:** Emission reductions needed to reduce PM<sub>2.5</sub> concentrations by  $2 \mu\text{g}/\text{m}^3$  at each airport's home grid cell.

## Chapter 5

### Conclusion

#### 5.1 Conclusions and Future Work

We have utilized HDDM-3D as implemented in CMAQ to quantify the impacts of both NAS-wide aviation emissions and airport-specific aviation emissions on the formation of  $\text{PM}_{2.5}$  and  $\text{O}_3$ . In this way, we can develop a deeper understanding of how varying aviation emissions may impact regional air quality and public health. The application of sensitivity coefficients to individual airports and precursor species allows for a more tailored approach in assessing health impacts as the aviation sector continues to grow. We found that 8.00, 18.41, 16.86, 7.05, and 11.77 times fewer emissions are needed at Hartsfield-Jackson Atlanta International Airport (ATL), Denver International Airport (DEN), John F. Kennedy International Airport (JFK), Los Angeles International Airport (LAX), and Chicago O'Hare International Airport (ORD), respectively to decrease concentrations of  $\text{PM}_{2.5}$  from nonattainment levels of  $14 \mu\text{g}/\text{m}^3$  to attainment levels of  $12 \mu\text{g}/\text{m}^3$  when considering all aviation precursors to  $\text{PM}_{2.5}$ . A  $2 \mu\text{g}/\text{m}^3$  decrease in  $\text{PM}_{2.5}$  is a large target to achieve when considering aviation emissions. This is why calculated emission reductions are large in our analysis. Since aircraft emissions are usually less than 1-5% of county-wide  $\text{NO}_x$  emissions, the general ranges of emissions reductions will be commensurate. We plan to expand this analysis for more airports in regions of nonattainment, as well as airports that are in regions of attainment to quantify the effects of aviation in relatively clean areas of the country. This will be done with 2011 emission data. We also plan to extrapolate our individual airport emission sensitivity results to sensitivities from aviation fuel burn. This can be used to help policy makers easily relate to aircraft operations at a given airport while designing effective policies.

#### 5.2 Acknowledgements

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